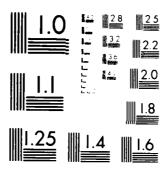
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NAVAL POSTGRADUATE SCHOOL Monterey, California



THESIS

ANALYSIS AND TESTING OF THE THERMAL DESIGN OF THE ELECTRONIC PACKAGE IN THE U.S. ARMY'S UPGRADED LOGIC MODULE (ULM)

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Henry C. Keebler III

September 1983

Thesis Advisor:

M. Kelleher

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20. ABSTRACT (Cantinue on reverse side if necessary and identify by block number)

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Analysis and Testing of the Thermal Design of the Electronic Package in the U.S. Army's Upgraded Logic Module (ULM)

by

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Captain, United States Army
B.S., United States Military Academy, 1973

Submitted in partial fulfillment of the requirements for the degree of

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ABSTRACT

The U.S. Army has developed an Upgraded Logic Module (ULM) for use in its Infantry Direct Fire Simulator System (IDFSS). It is designed to analyze data collected from associated instrumentation according to prescribed programming, to report results back to the system control via a telemetry interface, and it can be backpack mounted.

The thermal environment existing at Ft. Hunter Liggett,
Ca. (the primary operating environment for the ULM) during
the summer will add an abnormal thermal load to the ULM
operating environment in the backpack.

A mock-up of the actual ULM was built to model the heat dissipation of all the components and tested in different environments using extreme power consumption rates. The actual ULM was tested with typical power consumption rates and various environmental temperatures, including solar loading. Under typical operating conditions, the ULM will remain within manufacturer's tolerances for individual component temperatures. However slight increases in power consumption rates will severely stress the reliability limits of certain components, and the reliability of the entire system cannot be predicted.

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I. INTRODUCTION

A. BACKGROUND OF THE ULM

The U.S. Army Combat Developments Experimentation

Command (CDEC), conducts combat experiments at Ft. Hunter

Liggett, California, often involving infantry and vehicle

players in mock battle. These experiments are designed to

test various weapons systems, strategies, vehicles, and

personnel under equally varied conditions.

Players are generally instrumented to monitor the battle activity and are linked to a main computer system via telemetry devices. The instrumentation utilized must operate under dusty conditions, high vibration, and in temperatures ranging from 10 fahrenheit in the winter to 120 fahrenheit in the summer.

Prior to the experiment, player instrumentation is planned and designed to fit the particular parameters of the experiment. Maximum use of existing equipment is planned whenever possible. However, due to the uniqueness of many of the experiments—in terms of equipment and scope—new devices, cables, and mounting hardware must be designed or existing inventory modified. For these reasons and due to the high frequency of new experiments, there is a constant process of upgrading and re-designing existing equipment to meet the needs of the current experiment—with little regard given to the uses for future requirements.

The unfortunate consequences of this type of design process are many:

- Existing hardware--although functionally adequate-may not be compatible with other existing hardware.
- Due to modifications, documentation is often poor and usually only addresses the experiment of the original design.
- These poorly designed functional modules are extremely difficult for new personnel to use in the planning of new experiments.
- · Finally, much of the equipment has become obsolete and hard to maintain.

For these reasons CDEC has developed the Upgraded Logic Module (ULM) to replace the Logic Module of the Infantry Direct Fire Simulator System. The objectives of the ULM design are:

- Support the infantry player with minimum size and weight, yet allow expansion of functions where size and weight are not critical.
- · Fit the existing backpack.
- Use a microprocessor such that the inherent flexibility of the program memory can be used to meet future requirements without re-design.
- Provide input and output interfaces with sufficient flexibility to support the diverse player configurations.
- Be compatible with existing units and cables to the maximum possible extent.
- Use conventional packaging techniques to simplfy parts procurement, assembly, maintenance, and repair.
- · Provide hermetic sealing to protect against dust.
- · Provide general purpose bus interfaces for adding other developed equipment.

Partition the hardware and firmware into sharply defined functional modules to make the design easier to understand, to simplify the documentation, and to provide the ability to meet future requirements by redesigning a module instead of the entire ULM [Ref. 1].

B. OBJECTIVES

The thermal characteristics of the ULM were a prime consideration during the design process. Components chosen were specifically required to be capable of operation in the high temperature of the ULM. It was recognized that the small size of the ULM and the large number of integrated circuits could challenge the stress limits of current micr electronic packaging techniques [Ref. 2]. Additionally the high ambient temperatures existing at Ft. Hunter Liggett during the summer months would place an additional thermal load on the ULM which cannot be accurately predicted.

Thus the purpose of this test and analysis is to check the thermal performance of the ULM. Specifically tests were designed to:

- Determine if the ULM operating under typical conditions of power consumption and environment would remain within the reliability limits specified by manufacturers for their individual components.
- Attempt to predict performance under off-design conditions.

Using resistors to produce the heating characteristics of the individual internal components, a model was designed and constructed to simulate the power dissipation of the actual ULM. To accomplish the above objectives, both the

model and the ULM were instrumented with thermocouples to measure temperatures at specific locations and on specific components.

C. DEVICE DESCRIPTION

The Upgraded Logic Model (ULM) is an integral part of the Infantry Direct Fire Simulator System (IDFSS) responsible for the collection of data from infantrymen instrumented in connection with a combat development experiment. It analyzes data according to its programming for that experiment and reports results via a telemetry interface back to the system control computer center.

The ULM consists of two circuit boards housed in a machined cast aluminum case with outside dimensions of 1.75x5x10 in. The circuit boards are made of multi-layered glass epoxy and copper circuits. The fully populated boards and case weigh approximately five pounds. Its power consumption is rated at a maximum of 15 watts at 5 volts, with a typical usage of 7 to 9 watts at 5 volts [Ref. 3].

The case is made of two separate halves, each containing one of the circuit boards and one of the connectors shown in Figure 1.1. The half containing the J1 connector houses the CPU board, and the one containing the J2 connector houses the I/O board. The two boards are connected by a fifty pin ribbon connector, and when the two halves are assembled, the tops of the components from each board face each other. The

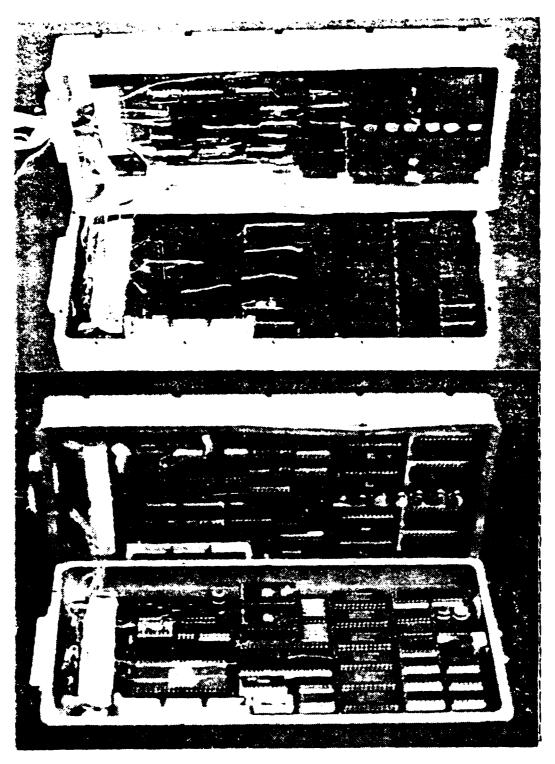


Figure 1.1 MODEL (top) AND TLM (bottom).

boards are fastened by 12 hex head machine screws with a gasket between the two halves of the case for dust protection.

The circuitry consists of a Central Processing Unit (CPU) Board and an Input/Output (.../O) Board, depicted in Figures 1.2 and 1.3. The CPU Board contains over 60 separate electronic components, including the 28002 16 bit CPU(u3).

The I/O Board also contains approximately 60 electronic components, including two Z-8 Micro-computer processors (u2,ull) and the ZCIO I/O chips(ul). The larger socket mounted dual-in-line pin (DIP) devices are listed in Tables 1 and 2, and are shown in Figures 1.2 and 1.3. All components are rated by the manufacturer for maximum case temperature tolerances to 125 C, except the following devices:

u3 of the CPU

ul,u2,ull,ul2, and ul3 of the I/O which are rated at 85 C.

The ULM is equipped with two connectors, one for power input and the other for I/O signals and testing. For this evaluation, the ULM was specially wired to give typical power consumption rates for the system without using the I/O connector. This allowed an I/O connector midification to accommodate the many thermocouple wires to be inserted into the case. However this also prevented the ULM from being tested under atypical power consumption rates.

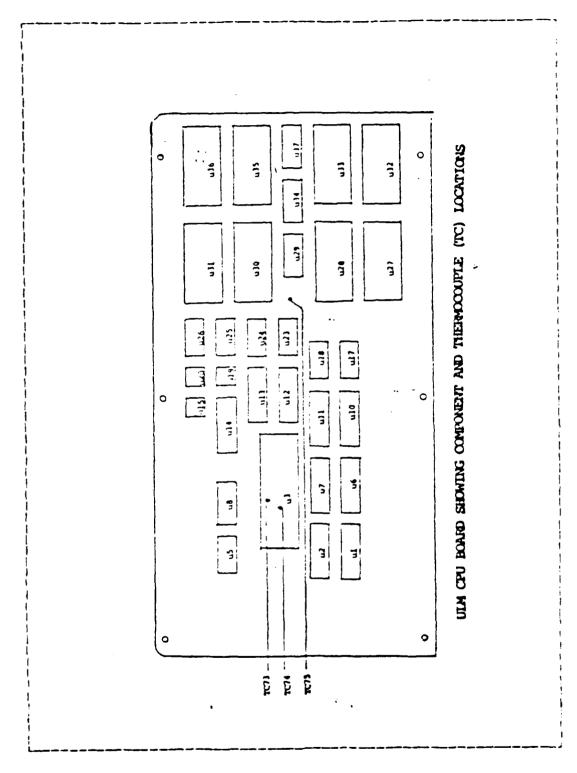
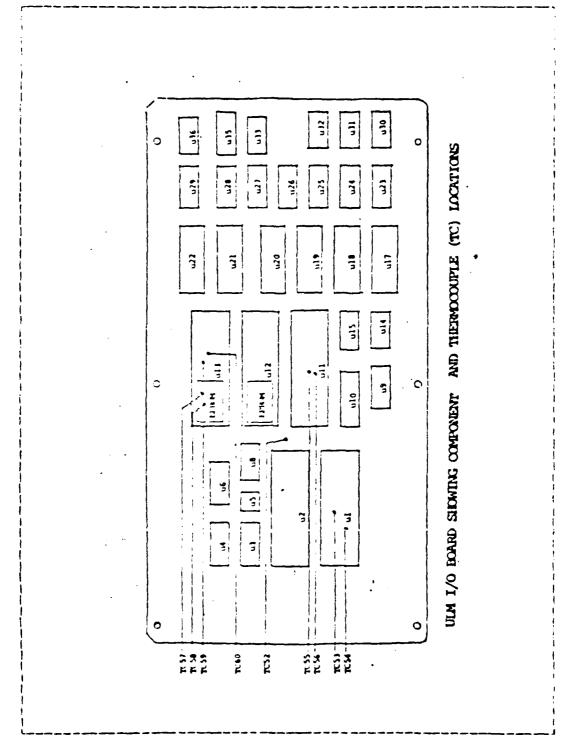


Figure 1.2 CPU BOARD.



Tipure 1.3 I/O BOARD.

TABLE 1
CPU MODEL DATA

UNIT	I(ma)	R(ohms)	POWER (w)
1	90	55.55	.45
2	90	55.55	.45
3	300	16.67	1.5
5	10	500.	.05
6	50	100.	.25
7	50	100.	.25
8	30	166.67	.15
10	90	55.	.45
11	90	55.	.45
12	40	125.	.20
13	120	41.66	-60
14	40	125.	.20
15-23	0	0	0
24	7	714.29	.04
25	6	833.33	.03
26	0	0	0
27	10	500.	.05
28	60	83.3	.30
29	0	0	0
30	60	83.3	.30
31	90	55.55	.45
32	10	500	.05
33	60	83.3	.3
34	0	0	0
35	60	83.3	.3
36	90	55.55	.45
37	0	0	0
38	40	125.	. 2

TABLE 2

I/O MODEL DATA

UNIT	I(ma)	R(ohms)	POWER (w)
1	250	20.0	1.25
2	250	20.0	1.25
3	0	0	0
4	0	0	0
5	50	100.	.25
6	0	0	0
8	0	0	0
9	26	192.3	.13
10	120	41.67	.60
11	250	20.	1.25
12	180	27.7	.90
13	180	27.7	.90
14-27	0	0	0
29	80	62.5	.40
30	54	92.6	.27
31	54	92.6	.27
32-36	0	0	0

II. TEST PROCEDURE

A. PRELIMINARY SETUP

Test procedures for the ULM and the model were determined by various limitations—primarily equipment availability and facilities. Initially, the actual ULM was not available for testing, and a model was presumed to be the primary vehicle for this analysis.

The questions were:

- How to fabricate the model to simulate the thermal characteristics of the ULM?
- How to instrument the individual components?
- How to simulate the various conditions under which the ULM would operate?

The last two questions also applied to the actual ULM when it was learned one would be available for testing. Fortunately, most of the solutions to these problems were equally applicable to the ULM, with only some modification.

Using an actual ULM case, two unpopulated ULM circuit boards, the ULM technical drawings, and power consumption rates--which were all provided by CDEC--the model was fabricated. To simulate the individual components in terms of thermal energy dissipation, resistors were used as heaters and scaled to the component's power dissipation rate shown in Tables 1 and 2. For most of the DIP components with 16 pins or less, DIP resistor networks were wired to meet the calculated resistance required and then

mounted into DIP sockets. Required resistances shown in Tables 1 and 2, were calculated based on power consumption rates of individual components at 5 volts. Using the relation:

power = current * voltage

the current was calculated, and using Ohm's Law:

voltage = current * resistance

an equivalent resistance was calculated for each component. For DIP components with more than 16 pins, the DIP resistor networks were not readily available. Therefore similar resistor networks were fabricated using single resistors wired into DIP adapters, forming an equivalent resistor network. Covers were added to these heaters to simulate a more even heat dissipation on the surface of the component, and to maintain geometric similitude. Each component was then placed in the exact position on the board as occupied by its actual counterpart.

Before beginning model fabrication, the decision to use type-T thermocouples for temperature measurement was made. As the critical temperatures for all components were well within the range of the type-T (copper constantan) thermocouples, and the thermocouple wire and connectors were readily available, this was a logical choice. Due to the small area of consideration and to minimize disturbances

to the internal natural convection of the air, 30 gauge wire was chosen for fabricating the thermocouples.

Next a determination was made concerning which specific components were to be instrumented. This was based on elements with the lowest critical temperatures and the highest heat dissipation from Tables 1 and 2. Additionally, thermocouples were placed on the boards, in the air gap between the boards, and on the inside and outside of the case to determine the various thermal resistances of the heat flow path. These locations are listed in Tables 3, 4, and 5 and shown in Figures 1.2, 1.3, 2.1, and 2.2. The thermocouples were fabricated in lengths of approximately 24 in. and connected to 15 ft. lengths of type T thermocouple extension wire.

The thermocouples were then calibrated using the HP 3054
Data Acquisition System and the Rosemount calibration bath
(see Appendix B). Two D-style 50 pin connectors used on
the ULM were also used on the model. One was used to
provide power to the unit, while the other was modified and
used as a passageway for the thermocouple wires. The modification was accomplished by drilling out 8 of the pins in the
center of the connector with space to accommodate the
bundle of thermocouple wires. A slit large enough for one
wire was cut in the top of the connector to the hole to
facilitate the removal and insertion of the thermocouple

Table 3

MODEL I/O BOARD THERMOCOUPLES (TC)

TC	COMPONENT/LOCATION
61	u2 bottom
62	u2 top
63	ul bottom
64	ul top
65	ul0 top
66	ulo bottom
67	ull bottom
68	ull top
69	ul2 bottom
70	ul2 top
71	ul3 bottom
72	ul3 top

MODEL CPU BOARD THERMOCOUPLES (TC)

<u>TC</u>	COMPONENT/LOCATION
41	u3 bottom
42	u3 top
43	board bottom vicinity u30 and u35
44	board bottom vicinity ul0 and ul7
45	inside wall of j2 (case)
46	inside wall of jl (case)
47	board top vicinity ul0 and ul7
48	board top vicinity u20 and u26
49	board top vicinity u30 and u35
50	board top vicinity u27 and u32
51	air vicinity u30 and u28
52	air vicinity u2 and ull

Table 4

ULM I/O BOARD THERMOCOUPLES (TC)

TC	COMPONENT/LOCATION
53	ul bottom
54	ul top
55	ull bottom
56	ull top
57	ul3 bottom eprom
58	ul3 top eprom
59	ul3 bottom
60	ul3 top

ULM CPU BOARD THERMOCOUPLES (TC)

$\underline{\mathtt{TC}}$	COMPONENT/LOCATION
73	u3 bottom
74	u3 top
75	air vicinity u30
76	air vicinity u38

Table 5
COMMON THERMOCOUPLES (TC)

TC	COMPONENT/LOCATION
45	J2 inside (case)
46	Jl inside (case)
53	ambient air for model runs after 13 AUG 1983see note
72	ambient air for ULM on 12 AUG 1983see note
77	ambient air for all runs prior to 13 AUG 1983see note
77	backpack air for all runs from 12 AUG 1982 see note
78	inside front wall of case
79	J2 outside (case)
80	Jl outside (case)

NOTE: Changes to thermocouple locations were required on 12 AUG 1983.

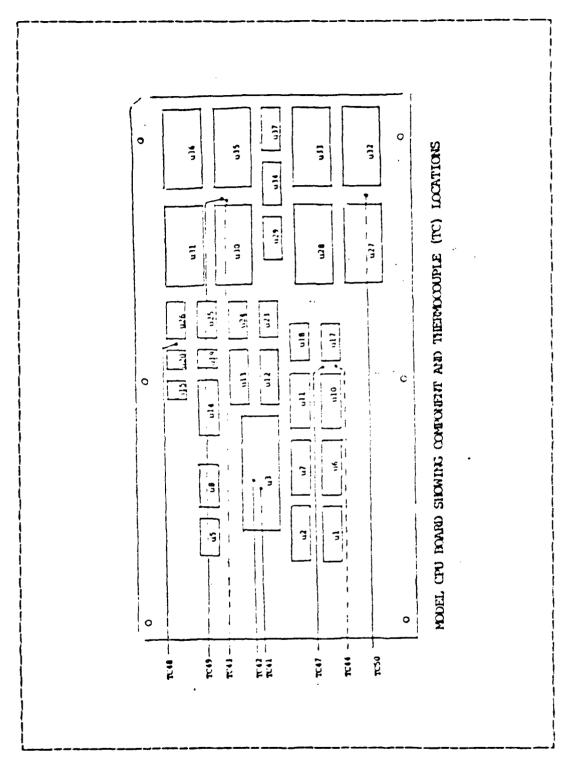


Figure 2.1 MODEL CPU BOARD.

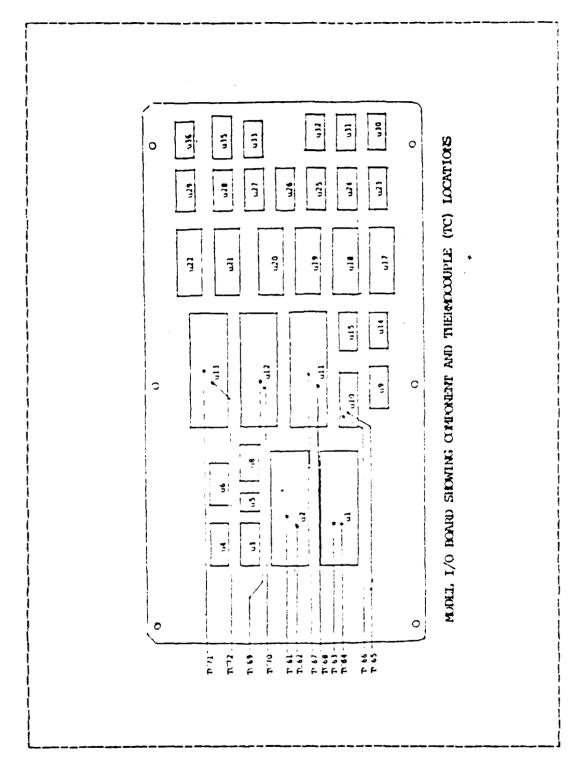


Figure 2.2 MODEL I/O BOARD.

wires individually. The unit was made almost air tight by packing the hole with silicon rubber sealant.

Power to the ULM was provided by a Lambda 60 volt power supply capable of voltage and current limitation. A Dana Digital Multimeter Model 4200 was used to monitor and adjust the power to the ULM/model, and check resistances. For gathering data, the HP3054 Data Acquisition System was utilized. It consisted of the HP3456 Digital Voltmeter for reading compensated EMF values from the thermocouples and the HP3497 Data Acquisition Control unit for controlling data flow. An HP 9826 computer was used to control the HP3054 and to store data on 5.25 in. floppy disks (see Appendix A).

The system was set up as follows:

- * A calibrated 2 ohm resistor was put in series with the load (model/ULM) to obtain accurate current measurements for calculating input power.
- A junction board containing a switch for reading the voltages of the resistor and the load was fabricated.
- The schematic is shown in Figure 2.3.
- · Power to the unit was controlled by the settings on the Lambda power supply.
- Temperature was measured by using the thermocouples, the HP3054 system, and the HP9826 computer. The schematic is shown in Figure 2.4.

The actual ULM circuit boards and a backpack became available for testing at this point. It was then decided that the actual ULM would be instrumented similarly to the

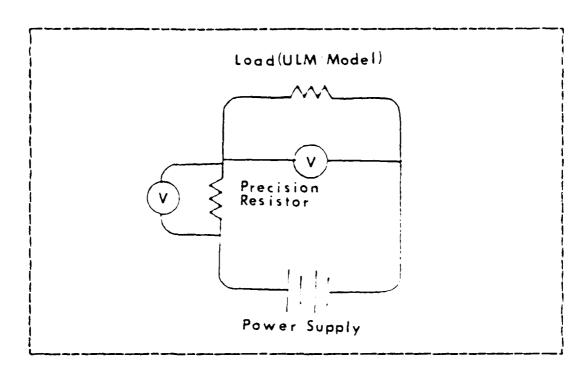


Figure 2.3 SCHEMATIC OF POWER SETUP.

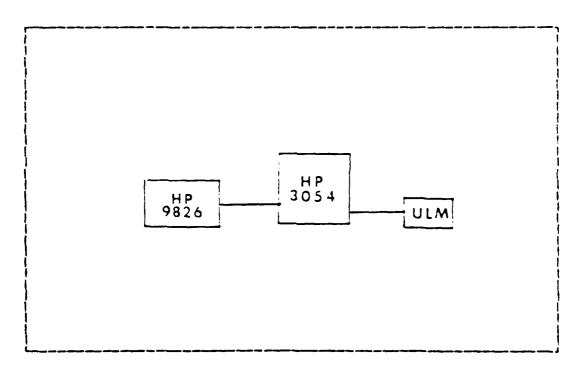


Figure 2.4 SCHEMATIC OF DATA ACQUISITION SETUP.

model. Unfortunately, the ULM could operate only in its typical operating range, and therefore could not be tested under max power ratings. An environmental chamber with variable temperature control was available for use. The environmental chamber had a maximum limit of 48.8C on its control system and was the size of a small room—approximately 40 square feet. This allowed the backpack and ULM to be placed within the chamber in a stabilized environment while being monitored and controlled from outside the chamber. The test procedure was implemented as follows:

- The ULM and model would be run under room temperature conditions to test for proper operation of the systems and to ascertain the operating characteristics of each.
- The ULM would then be installed in the environmental chamber to determine the ambient temperature at which critical temperatures would be reached.
- The ULM and data acquisition system were then transported to Ft. Hunter Liggett on a typical summer day for testing in the ULM's actual environment.
- The model then replaced the ULM in the backpack and tests were again conducted in the environmental chamber. This time runs were conducted in an attempt to exactly simulate power and environmental conditions of all the ULM tests.

B. CONDUCT OF TESTS

This section will cover the specific procedures of all runs performed in the analysis. Data from the runs are contained in Appendices D through G. 40 thermocouples were assembled and divided between the ULM boards, model

boards, the case, and external locations, which are listed in Table 3. Programs were written to automate the data acquisition process. All programs were in Hewlett Packard Basic 2.0 programming language. Specific programs were written for:

- Data acquisition and storage during the calibration procedures. These are contained in Appendix B.
- Calculation and storage of second order polynomial coefficients for calibration corrections of each thermocouple. This program is listed in Appendix B.
- Data acquisition and storage of temperatures for each thermocouple of the model. This program is in Appendix C.
- Data acquisition and storage of temperatures for the ULM thermocouples. This program is listed in Appendix C.

The data acquisition programs for the model and the ULM were interactive and required the following input:

- Month, day, hour, minute and second of the start of the run. This was required to set the internal clock of the HP 3497 control device.
- . Voltage readings for the load and the calibrated resistor for calculation of the power and current values.
- · The time interval for the wait between data sets.
- · Number of data sets to be taken automatically.

The ULM model was first tested on 16 July 1983 in Halligan Hall, room 103. Using the setup previously explained, the model was placed on its side on a wooden board. The ambient temperature of the room was 24C (73F). The purpose of the test was to:

- · Check the operation of the model and the system.
- Obtain data for further planning of test procedures. After studying initial data, it was obvious some of the heaters were not operational. The overall resistance of the system was approximately 3.1 ohms and was checked before and after the tests. However, when power was applied, some of the solder connections were non-conducting electrically. This required resoldering and reassembly of the model boards. The next test for the model was conducted on 18 July 1983 in the same location and under the same conditions as the first test. Power was set at 10.71 watts, and 10 runs were taken at 60 minute intervals. Power was increased to 15 watts--the maximum power level predicted by CDEC for their critical maximum temperature of 85 C. Therefore, to prevent damage to the components, this test was terminated. An examination of this initial data taken at room temperature indicated that if the ULM and the model were to react similarly, the ULM would have problems operating in extreme conditions.

On 26 July the first ULM test was conducted for the same purpose as the first test on the model. However, this test was conducted with the ULM instrumented and placed inside the backpack. The pack was placed in a horizontal position in the same location and under the same conditions as the model test. 10 readings were taken at 5 minute intervals to obtain transient temperature data. Power was

set at 8.72 watts. Next, 8 readings were taken at 30 minute intervals to obtain steady state data. The settings resulted in a power level of 8.71 watts. Since power could not be incremented to maximum on the ULM, lower temperatures—as compared to the model—were obtained on the ULM.

It was noticed there was a danger of cutting the thermocouple wires when inserting and extracting the module to and from the backpack. Therefore it was decided to complete all tests on the ULM before conducting tests on the model. The environmental chamber was then modified to accept the cabling for control of the power and thermocouples. It was heated to 48.8C (120F), the maximum setting for the chamber. For this temperature, it generally took 3 days to reach a constant internal temperature; therefore it was decided to start at this maximum setting. If this was too extreme for the ULM it would be faster to cool down the chamber than to heat it.

On 1 Aug 1983 the ULM was tested in the environmental chamber with the backpack in an upright position (this would be the usual position when carried by an instrumented soldier). 8 samples were taken in 5 minute intervals at a power level of 8.09 watts. 20 readings were then taken in 30 minute intervals with a power level of 7.59 watts at the same settings. The maximum temperature achieved was 78C (173F) on the CPU (u3). It was evident that none of

the components would reach their critical temperatures under these conditions at typical power levels.

The ULM's next test was conducted at Ft. Hunter Liggett, Ca. on 12 Aug 1983. This was done to determine the effect that solar loading in the actual environment would have on the system. The backpack was placed in direct sunlight on a concrete pad in a vertical position. This test was started at 0800 hrs. and ended at 1500 hrs. on a typical summer day for that region. Ambient temperatures were taken from a location in the shade near the backpack. Some tests were initially taken to examine the sun's effect on internal pack temperatures. 10 samples were taken at 5 minute intervals with the ambient temperature ranging from 21.4C to 23.7C. Power was turned on, and 15 readings were taken at 5 minute intervals at a power level of 7.93 watts. The ambient temperature ranged from 24.1C to 29.1C. Next, 10 samples were taken at 15 minute intervals with power now at 7.56 watts. Ambient temperature for this run ranged from 30.3C to 34.5C. Due to the changing direction of the sun's rays, the backpack was reoriented to maintain full irradiation by the sun. This required moving the backpack off the concrete slab onto the dirt. 8 samples were then taken at 15 minute intervals with power at 7.44 watts with no change to the power settings. Ambient temperature ranged from 35.2C to 37.4C. Again none of the components reached its critical temperature. This completed testing of the ULM.

Returning to the Naval Postgraduate School, the model was placed in the backpack and tests were conducted in the environmental chamber to duplicate -- for comparison -conditions of the ULM tests. On 14 Aug 1983 the model was tested with 8 samples taken at 5 minute intervals and a power level of 7.9 watts. Ambient temperature was at 43.3C for this run. Next, 20 samples were taken at 15 minute intervals at the same power level. On 15 Aug 1983 the temperature was set to 48.8C to duplicate the ULM's run on 1 Aug 1983. 8 samples were taken at 5 minute intervals at a power level of 7.91 watts. 20 samples were taken at 15 minute intervals, with power now at 7.97 watts. The final test run was taken--also on 15 Aug 1983--at 37.7C for obtaining data to compare steady state with and without solar loading at the same ambient temperature. 15 samples were taken at 5 minute intervals and power set at 7.72 watts. Next, 24 samples were taken at 30 minute intervals with power now at 6.62 watts.

III. EVALUATION OF RESULTS

A. RESULTS

Results are presented in this section with a summary of the observations of each test followed by the corresponding graphs produced from test data. The graphs depict the thermocouple temperatures plotted against time with either ambient or backpack temperatures, or both, shown for comparison purposes.

The test on 1 August 1983 was conducted at a constant temperature of 48.8C in the environmental chamber. The following are observations from data taken during these runs:

- · None of the susceptible components reached its critical temperature of 85C.
- Max steady state temperatures achieved are shown in Figures 3.1 to 3.3 and are listed here as:

```
ull = 77.2C
u3 = 78.6C
ul3 = 72.8C
ul = 61.1C
```

- Steady state was achieved at between 130 and 140 minutes after power was applied.
- Temperatures of internal and external portions of the case are:

```
internal J1 (TC46) = 56.0C external J2 (TC80) = 54.4C
```

There were no unexpected trends or observations resulting from this test.

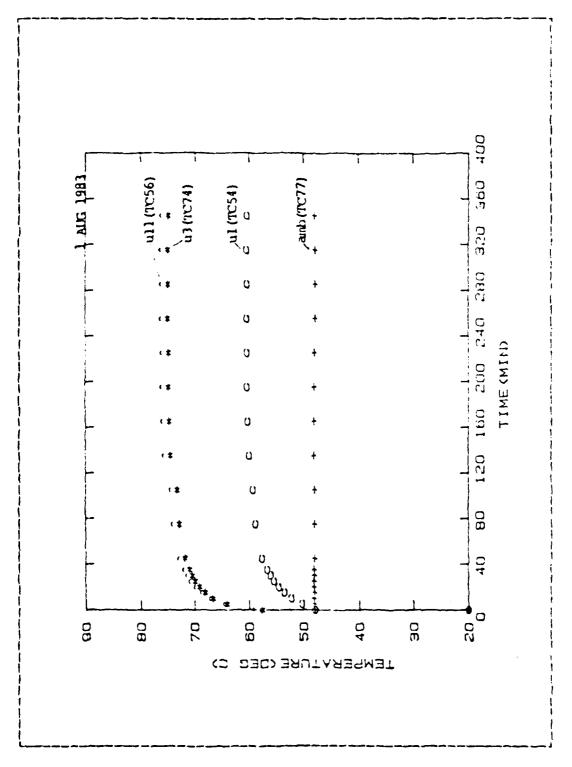
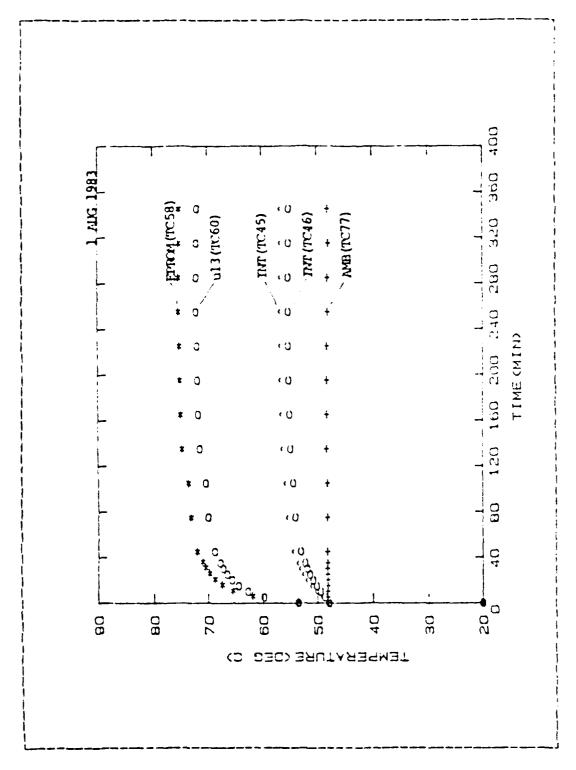


Figure 3.1 1 AUGUST 1983 - graph 1.



Pigure 3.2 | 1 AUGUST 1983 _ graph 2.

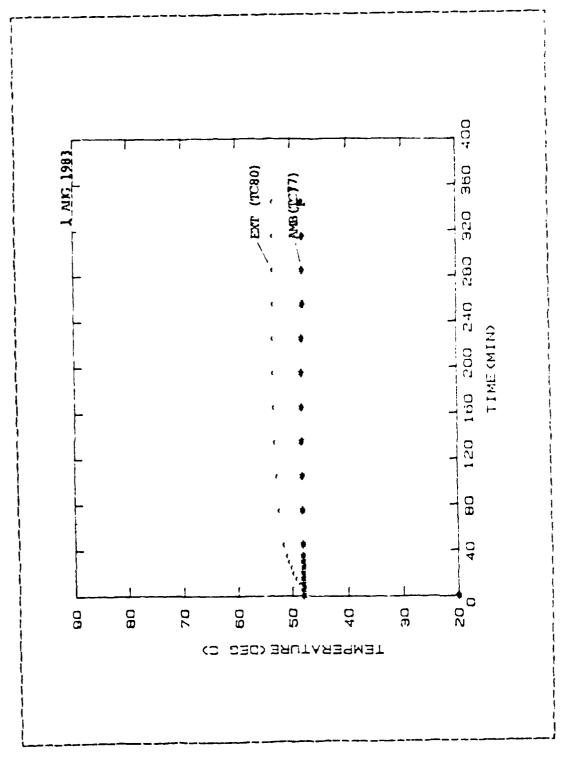


Figure 3.3 1 AUGUST 1983 - grapa 3.

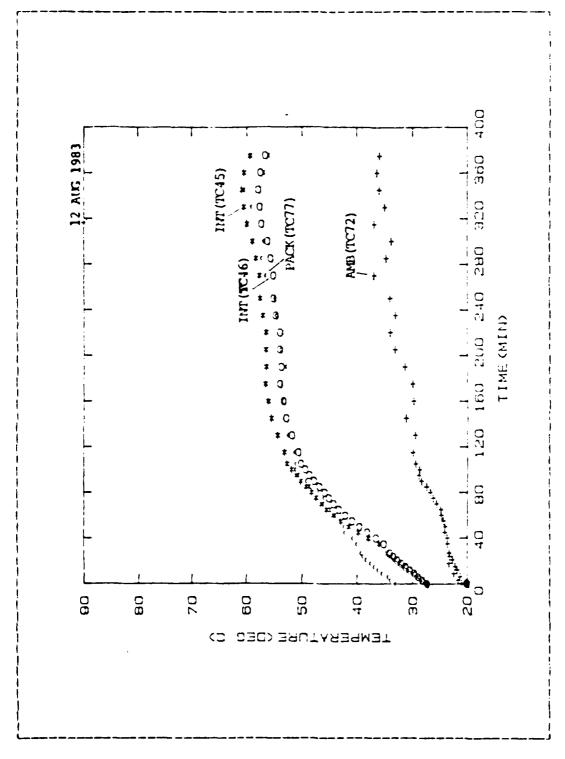
The test conducted at Ft. Hunter Liggett experienced ambient temperatures ranging from 21C to 38C and fluctuated due to occasional wind currents. This test began at 0800 hrs. on 12 August 1983, and terminated at 1530 hrs. on the same day. The following was observed:

- None of the susceptible components reached its critical temperature of 85C.
- Max steady state temperatures acheived are shown in Figures 3.4 to 3.8 and are listed here as:

ull = 78.78C u3 = 79.16C ul3 = 78.4C ul = 64.3C

- The internal pack temperature reached a maximum of 60.8C--22.8C above ambient--as a result. of solar loading and internal heat produced by the ULM.
- Although steady state was not reached (due to ambient temperature fluctuations), the effects of transient heating appears to have taken between 130 to 140 minutes. This is due to the heating by the components as opposed to external solar loading.
- Apparently, moving of the pack disturbed the external thermocouple (TC80) causing it to give spurious readings after 250 minutes as seen in Figure 3.5. This is most likely a result of loose connections at the thermocouple connectors.
- The sudde jump in temperature at 30 minutes (for TC's 54, 56, 50, 60 and 74) is a result of the power switch being turned on. Temperature increases prior to 30 minutes are due only to the effect of solar radiation on the backpack.

The first 15 August 1983 test on the model was conducted in the environmental chamber at an ambient temperature of 48.8C. Observations resulting from this test are:



Pigure 3.4 12 AUGUST 1983 - graph 1.

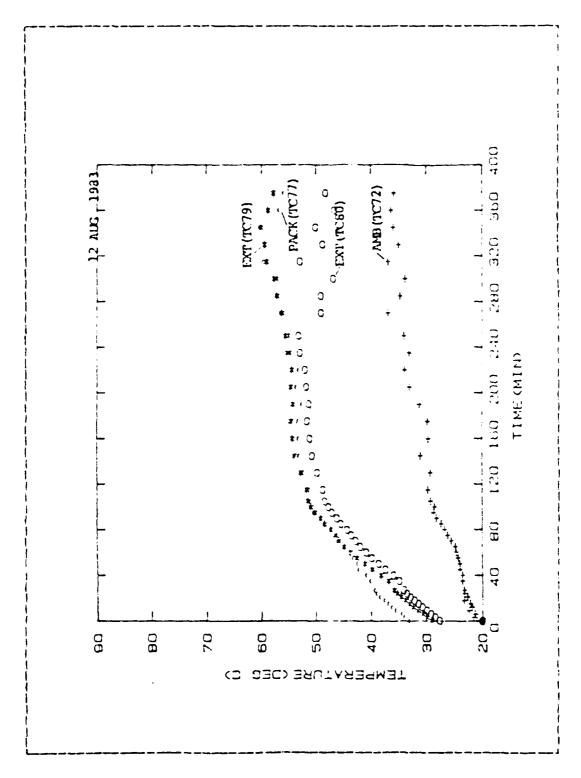
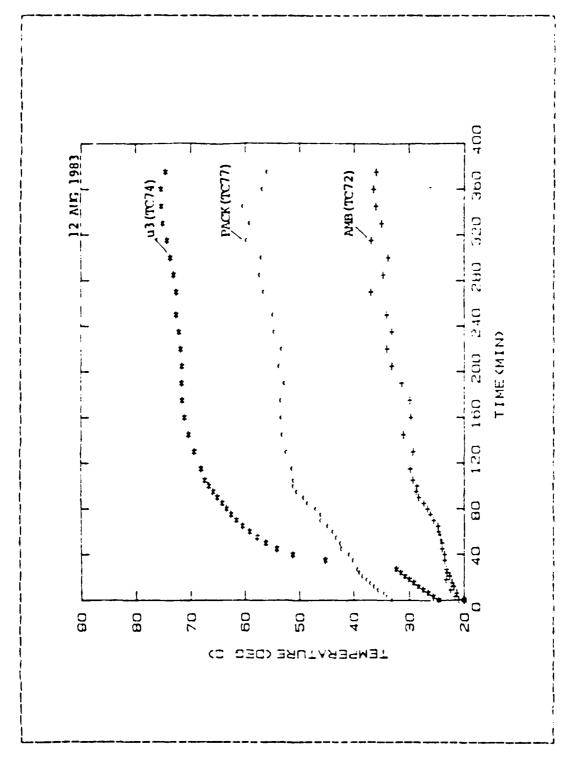


Figure 3.5 12 AUGUST 1983 _ graph 2.



Pigure 3.6 12 AUGUST 1983 - graph 3.

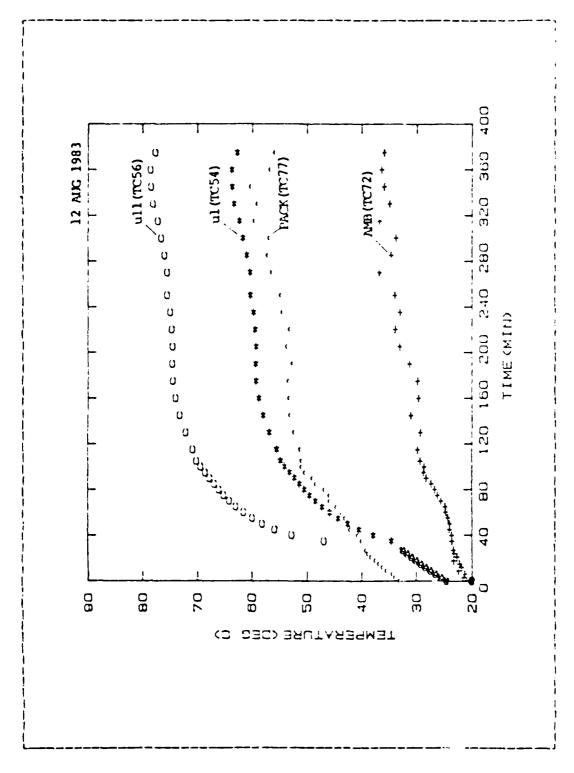


Figure 3.7 12 AUGUST 1963 _ graph 4.

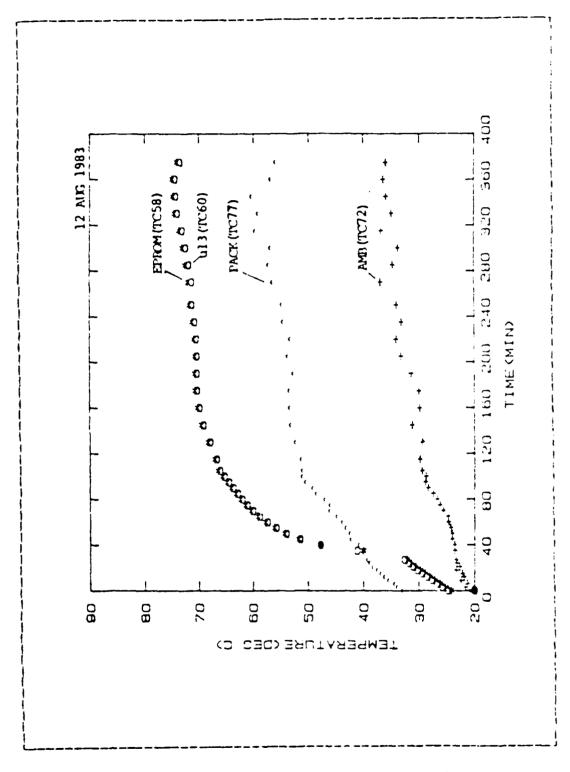


Figure 3.8 12 AUGUST 1983 - graph 5.

- None of the susceptible components reached its critical temperature of 85C.
- Max steady state temperatures achieved are shown in Figures 3.9 to 3.11 and are listed here as:

ull = 76.11C u3 = 66.80C ul3 = 77.54C ul = 84.58C

- As a result of internal heat produced by the ULM, the internal pack temperature reached a maximum of 54.8C--6C above ambient.
- Unexpected temperature fluctuations occurred at 45, 120, and 300 minutes on TC's 42, 64, 68 and 72. Since the only thermocouples experiencing these fluctuations were attached to powered components, this may have been caused by a power fluctuation of the power supply.

The second test of the model on 15 August 1983 was conducted again in the environmental chamber set this time to an ambient temperature of 37.7C. Observations from this test are:

- None of the susceptible components reached its critical temperature of 85C.
- Max steady state temperatures achieved are shown in Figures 3.12 to 3.14 and are listed here as:

ul1 = 60.22C u3 = 52.33C ul3 = 63.60C ul = 68.78C

- As a result of internal heat produced by the model, the internal pack temperature reached a maximum of 41.1C.
- Steady state was achieved between 80 and 120 minutes after power was applied.
- Unexpected temperature fluctuations occurred in TC's 53 and 68, between 5 and 15 minutes. These fluctuations cannot be explained.

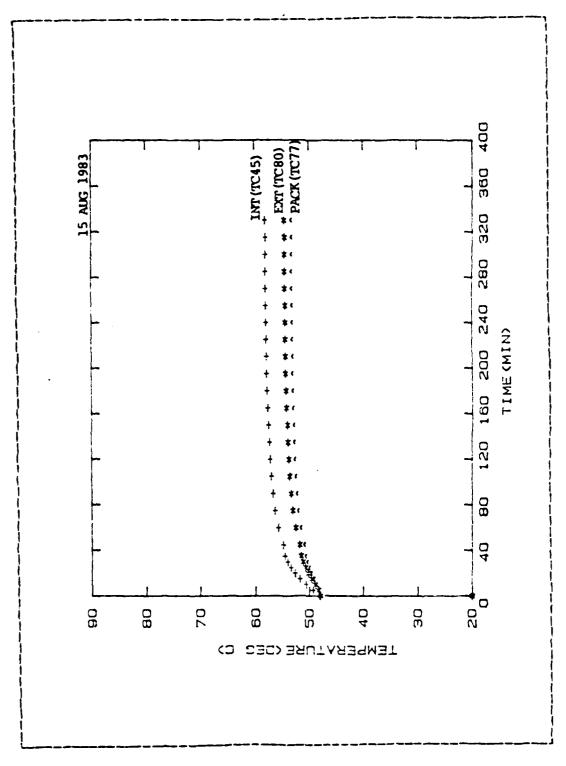


Figure 3.9 15 AUGUST 1983 (AMBIENT = 48.8C) - graph 1.

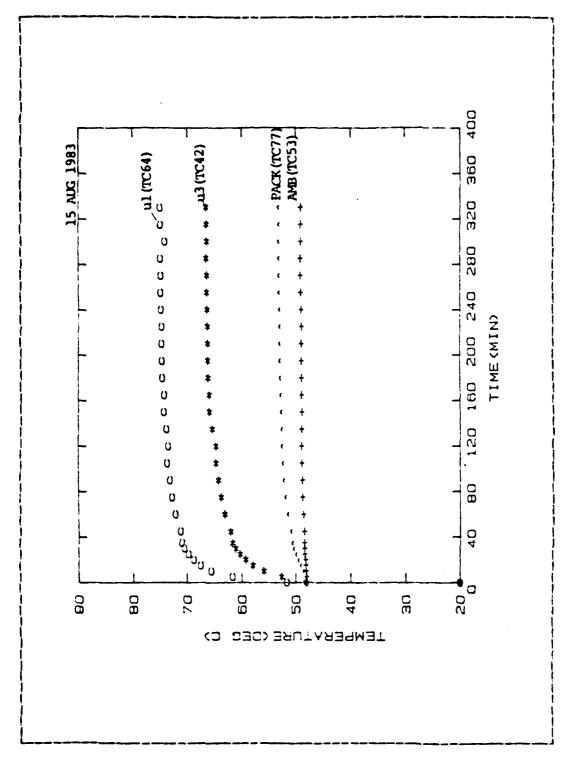


Figure 3. 10 15 AUGUST 1983 (AMBIENT = 48.8C) - graph 2.

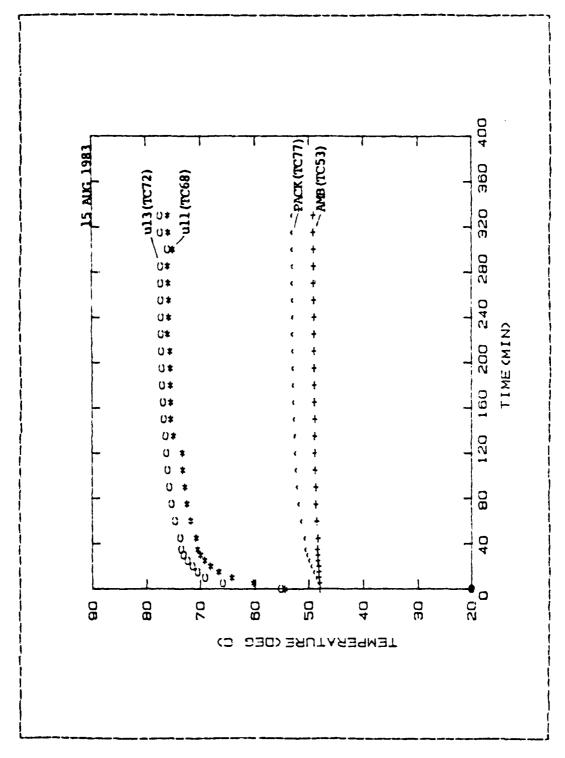


Figure 3.11 15 AUGUST 1983 (AMBIENT = 48.8C) - graph 3.

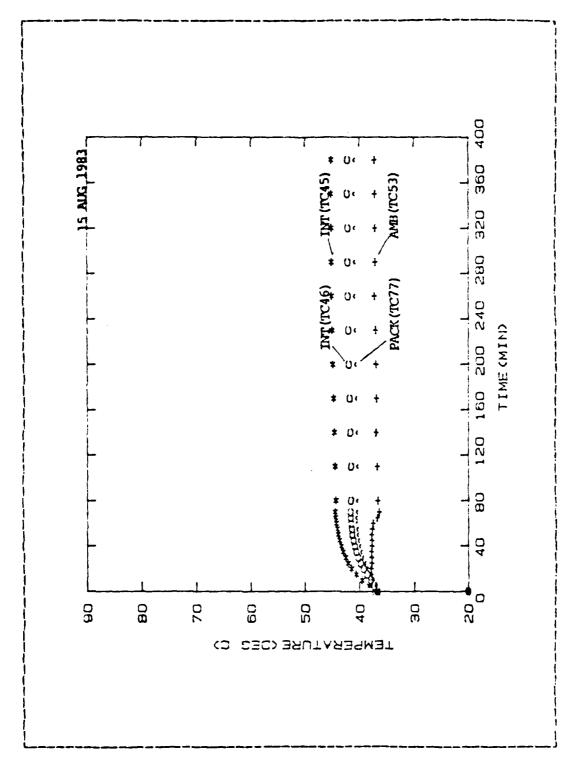


Figure 3.12 15 AUGUST 1983 (AMBIENT = 37.7C) - graph 1.

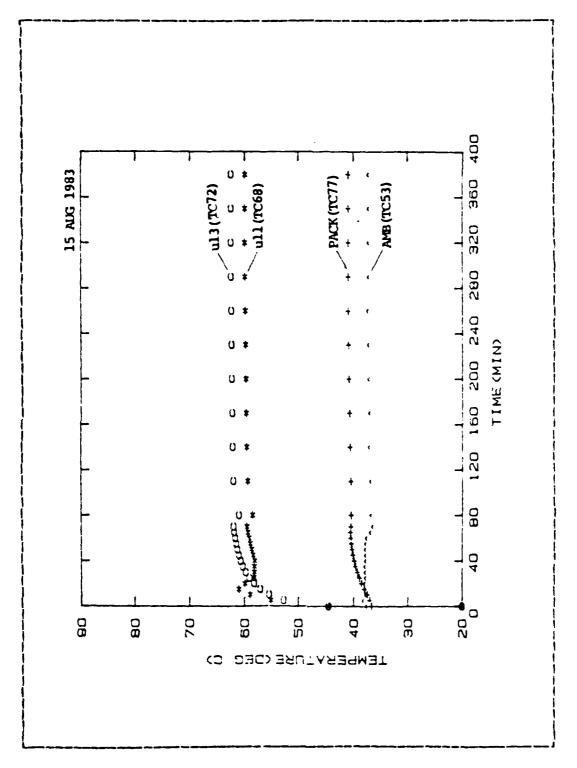


Figure 3.13 15 AUGUST 1983 (AMBIENT = 37.7C) - graph 2.

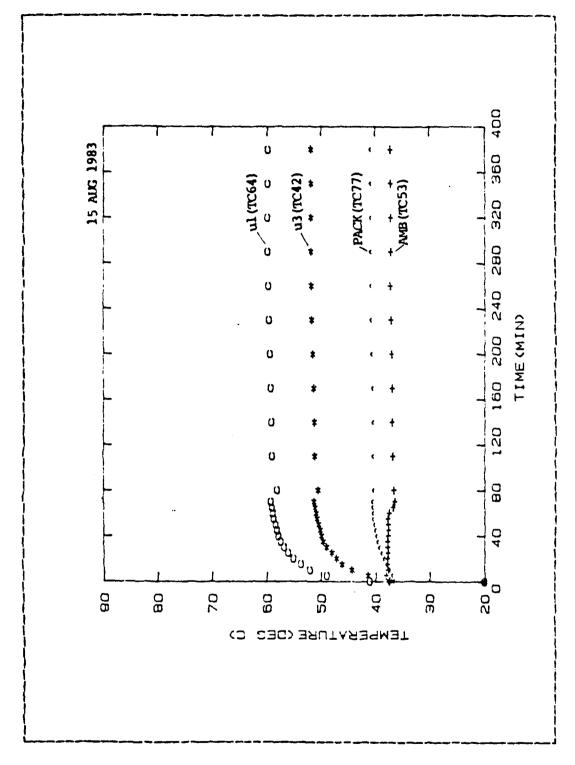


Figure 3.14 15 AUGUST 1983 (AMBIENT = 37.7C) - graph 3.

Unexpected temperature fluctuations occurred in all thermocouples between 50 and 80 minutes. It appears that all the fluctuations lag slightly behind that of the ambient air fluctuation. An actual change in ambient air temperature would have this type of delayed response. Since the environmental chamber was not monitored continuously, the door may have inadvertently been opened, or there may have been a short loss of power to the heating system of the chamber.

B. DISCUSSION

The ULM and backpack will be subjected to ambient environments ranging typically from 21C to 38C during the warm summer season. Solar loading--typical of a Ft. Hunter Liggett summer day--could add 22C higher environmental temperatures within the backpack resulting in a higher stress experienced by the ULM.

Energy in the form of heat will naturally flow from a hot element to a colder one. The rate of heat flow (Q) is proportional to the temperature difference (2T) and inversely proportional to the thermal resistance ($\frac{1}{2}$) of the medium through which the heat is flowing. This relationship is:

 $Q = (\Delta T) / \theta$

In the ULM--as in most electronic equipment--most of the energy used to power the equipment is converted to heat, causing the equipment temperature to rise. The temperature will continue to rise unless the heat can be removed. In the ULM, the power input to the module is the

total energy that must be dissipated. In the case of the ULM, the ultimate sink for thermal energy is the air outside the backpack. Both the air inside the backpack and the backpack itself, can be considered local sinks through which all energy leaving the ULM must flow [Ref. 4].

There are three modes of heat transfer at work in most systems:

- Conduction refers to heat transfer across a medium resulting from kinetic energy interchange between molecules or by electron drift [Ref. 5]. Conduction can occur in a solid, liquid, or gas and is the only mode of heat transfer occurring in an opaque solid [Ref. 4].
- * Convection heat transfer occurs at the interface between a solid and a fluid at a different temperature when fluid motion is present. The fluid of this analysis is air. Motion caused by the density differences associated with the temperature variation within the fluid is called natural convection. Motion caused by external methods is forced convection. In this analysis the only forced convection is when wind is present [Ref. 5].
- Radiation heat transfer refers to the energy emitted by matter in the form of electromagnetic waves. Given two surfaces at different temperatures, each will be emitting and exchanging thermal radiation. However, the net radiation exchange is in the direction of hot to cold and will continue until both surfaces are the same temperature. At this point the net radiation will be zero [Ref. 6]. The net radiation occurring between two bodies with similar surface material, is a function of the intensity which varies with the viewing direction between the emitting surfaces. Thus the energy transferred from one surface to another is a function of the area of the receiving surface "seen" by the emitting surface [Ref. 5].

The primary heat flow paths of this system are:

 From each component to the ULM case via convection and conduction.

- From ULM case to backpack by convection through the air, by conduction through the backpack frame, and by radiation.
- · From backpack to ambient air via forced and natural convection, and radiation.

Because of the geometric positioning of the components, radiation was not considered as playing a very significant role in the component to ULM case heat flow path. The dissipating elements are flat DIP devices whose sides make up a small proportion of emitting surface. The greatest surface area is the top of each component. When assembled, each of these surfaces is facing another dissipating surface. This would have an effect of heating the lower temperature device, but as both are power dissipators, the net effect in terms of energy dissipation would be negligible.

Natural convection and conduction would be the primary heat transfer modes of energy transfer from the component to the air. Since the ULM was hermetically sealed, the only fluid motion would be caused by natural convection. The dense packing of the components leaves little room for temperature gradients to occur between components on the same board. The space between the boards and the top surfaces of the components vary with the component. Some components would act as barriers to air flow resulting from adjacent components. Unfortunately, all high power dissipating components are clustered at one end of the ULM.

Additionally, the hot components of the I/O board directly face the hot components of the CPU board. Since the air is being heated from two directions, the cooling effect of the air on the surface of each component is reduced. Thus, due to the geometric configuration and high concentration of high power dissipators, it is postulated that much of the advantage in cooling achieved by natural convection is offset by the dual heating effect. This would leave conduction as the dominant heat transfer mode within the ULM.

Conduction within the ULM will occur from component to air to the case, and component to board to the case. Since the boards are separated from the case by electrically insulating gaskets, most of the conduction will take place from boards and components to the air--then to the case. With the available data, however, it is impossible to quantify how much heat is conducted by the boards to the case compared to conduction from the components to the case.

Ideally all thermal paths with their individual resistances would be calculated. However, the complexity of this device and amount of instrumentation required for this type of analysis made such a task impractical. It would have required calculating not only the path of the energy from each component to the ultimate sink, but also

the effect each of the other components would have at each temperature along the path. Even if the device could be instrumented to determine all of these temperatures, the individual power dissipating rates for each component of the actual ULM would have to be available. This data was not available. Unfortunately there is little correlation between the behavior and resistances of IC components and the resistors used to model the components. This is because power dissipation in the IC components is frequency dependent and not based solely on voltage supplied to and the resistance of the component. This is the case for the model, which is made of resistors having a fixed value. Thus little correlation existed between the actual component and its model, in terms of individual power dissipation. Knowing the total dissipation of the ULM enabled calculating an equivalent thermal resistance from the internal backpack air to the ambient air shown in Figure 3.15. These calculations are based on the following assumptions:

- The temperature measured inside the backpack is assumed to be representative of the average value of the air within the backpack.
- Heat dissipated by the backpack frame directly to the ambient air is assumed to be negligible compared to the heat dissipated by the internal backpack air through the canvas to the ambient air.

Using data from the environmental chamber on 13, 14, 15 August, 1983, and the relation:

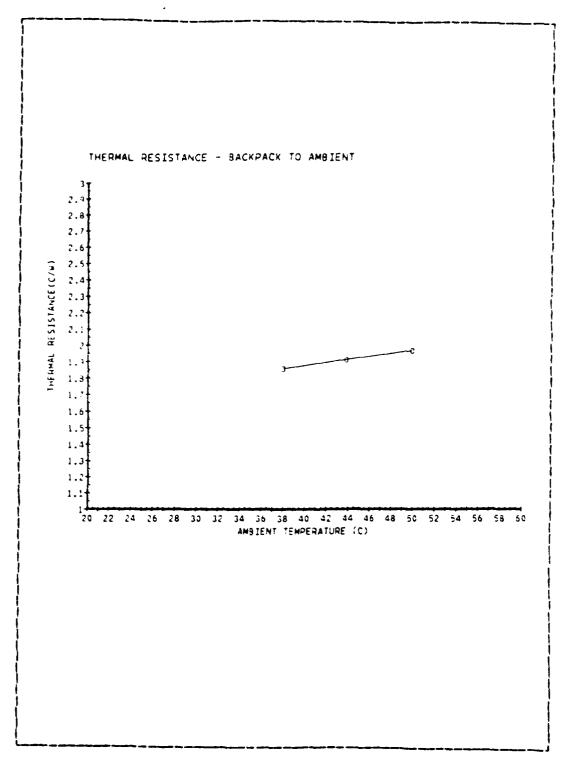


Figure 3.15 THERMAL RESISTANCE OF PACK AIR TO AMBIENT.

Theta was calculated as 1.86 C/W for the test of 12 Aug 33. Therefore, since the total heat within the pack was the sum of the ULM load and the solar load, the solar load was calculated as 29.67 watts. This is as if in the absence of solar loading, the ULM--at 8 watts--was joined in the backpack by an additional unit of 30 watts. This is a very significant additional thermal stress

C. CONCLUSION

Operating under typical power consumption rates

(approximately 8 watts) under design environmental conditions of Ft. Hunter Liggett in the summer, all internal components were measured to be below their specified critical temperatures of 85C or higher. The design conditions meant here are:

- An environmental temperature range of 21C to 38C (70F to 100F)
- · The ULM mounted in a backpack
- · No additional internal heat sources
- · The backpack in direct sunlight
- · No wind.

However, operating under these conditions causes several of the components, whose critical temperatures are 85C, to be within 5 to 10C of that limit. Therefore, any slight increase in power over 8 watts, or increase in ambient

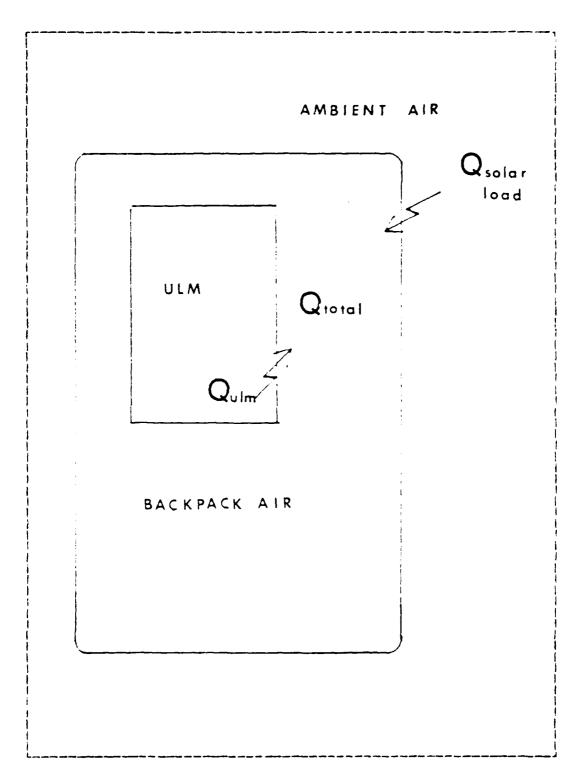


Figure 3.16 ENERGY BALANCE ON THE BACKPACK.

temperature above 38C, could cause one or more of the components to exceed specifications. Then reliability of the system could not be predicted, and would be substantially decreased. Conversely, the absence of direct sunlight and/or the addition of wind would have a beneficial effect on the ULM by decreasing the thermal stress on the unit.

APPENDIX A

EQUIPMENT LIST

The following is a list of the equipment used for this analysis:

- Thermocouples were made of copper-constantan, 30 gauge, teflon coated thermocouple wire.
- The HP3054A Automated Data Acquisition System was used for data acquisition which consists of:

HP3497 Data Acquisition Control Unit

HP3456 Digital Voltmeter for obtaining data from the thermocouples

- The HP9826 Desktop computer was used to control data acquisition, storage of data, computation and display of data.
- The Lambda 60 volt power supply was used to provide power to the ULM and model.
- · A Controlled Acoustic Environmental Chamber manufactured by Industrial Acoustics Company Inc. was used for simulating ambient temperatures up to 48.8C (120F).

APPENDIX B

THERMOCOUPLE CALIBRATION

The following is a list of equipment used during the calibration of the thermocouples:

- Rosemount Engineering Model 920a Commutating Bridge
- Rosemount Model 162 Platinum Resistance Temperature Standard
- · HP3054 Data Acquisition System
- · HP9826 Desktop Computer

A computer program listed on page 62 was written for the HP9826 to:

- · Read emf values from the thermocouples
- · Store the emf values in a data file
- * Convert the emf values to temperatures based on a reference relative to platinum at OC.
- · Compare these temperatures to temperatures obtained from the platinum resistance standard.

A second program was written to fit a second degree polynomial to the comparison above and for obtaining coefficients to apply to each thermocouple. This program is listed on page 63.

The thermocouples and the platinum resistance standard were placed in the calibration bath. The temperature of the bath was cycled from 10C to 100C and back to 10C. Temperature measurements were taken at 20 degree increments

ascending and descending the scale. Coefficients correcting the thermocouple temperatures to the standard temperatures were calculated and listed on pages 64-67.

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2 DIM Emi(39).TCU9).Delta(39).Sx(39).Sx(39).Sx2(39).Sx2(39).Sx4(39).Sxy(39)

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COEFFICIENT -3.1930275E-01 1.0128575E+00 -5.4818475E-05	COEFFICIENT -2.2522528E-01 1.0107620E+00 -4.5712065E-05	COEFFICIENT -1.9938344E-01 1.0095769E+00 -4.1260696E-05	COEFFICIENT -2.4667796E-01 1.0108583E+00 -4.6423785E-05	COEFFICIENT -2.5058039E-01 1.0104461E+00 -4.3850226E-05	COEFFICIENT -1.4662748E-01 1.0081341E+00 -3.3403832E-05
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EXPONENT 0 1 2	COEFFICIENT -3.2936623E-01 1.0102503E+00 -4.3399839E-05	*2/1	54	EXPONENT 0 1 2	COEFFICIENT -2.9769225E-01 1.0095916E+00 -4.1222481E-05	= 2/1	09
EXPONENT 0 1 2	COEFFICIENT -3.5742917E-01 1.0111652E+00 -4.7246171E-05	=2/1	55	EXPONENT 0 1 2	COEFFICIENT -2.7987174E-01 1.0121568E+00 -4.9924368E-05	1/C=	61
EXPONENT 0 1 2	COEFFICIENT -4.1638880E-01 1.0117568E+00 -4.8533907E-05	-3/1	56	EXPONENT 0 1 2	COFFICIENT -1.9282761E-01 1.0102605E+00 -4.2767110E-05	1/C-	62
EXPONENT 0 1 2	COEFFICIENT -3.6276984E-01 1.0105931E+00 -4.4865618E-05	1/C=	57	EXPONENT 0 1 2	COEFFICIENT -2.1019688E-01 1.0103867E+00 -4.4603609E-05	1/C-	63
EXPONENT 0 1 2	COEFFICIENT -3.3989581E-01 1.0102587E+00 -4.4930951E-05	-3/1	28	EXPONENT 0 1 2	COEFFICTENT -2.4817587E-01 1.0112909E+00 -4.8233817E-05	1/C=	64

7	72	73	74	75	92
* 2/1	=3/1	1/C=	1/C=	- 2//1	1 /C•
COEFFICIENT -3.4055123E-01 1.0121429E+00 -4.9454810E-05	COEFFICIENT -2.2716454E-01 1.0104838E+00 -4.5364118E-05	COEFFICIENT -3.4035121E-01 1.0119056E+00 -4.9277126E-05	COEFFICIENT -3.3760097E-01 1.0126166E+00 -5.3815004E-05	COEFFICIENT -3.5448472E-01 1.0124541E+00 -5.0742084E-05	COEFFICIENT -3.4015128E-01 1.0118546E+00 -4.8928220E-05
EXPONENT 0 1 2	EXPONENT 0 1 2	EXPONENT 0 1 2	EXPONENT 0 1 2	EXPONENT 0 1 2	EXPONENT 0 1 2
99	99	29	89	69	70
1/6-	- 2/1	1/0-	1/C=	1/C-	- 2/1
COEFFICIENT -1.9101588E-01 1.0104827E+00 -4.5500415E-05	COEFFICIENT -2.6448185E-01 1.0116511E+00 -5.0080800E-05	COEFFICIENT -1.7570321E-01 1.0100325E+00 -4.4527871E-05	COEFFICIENT -2.7670041E-01 1.0119687E+00 -5.0293806E-05	COEFFICIENT -3.3189622E-01 1.0129848E+00 -5.4476114E-05	COEFFICIENT -2.3237513E-01 1.0108945E+00 -4.6776910E-05
EXPONENT 0 1 2	EXPONENT 0 1 2	EXPONENT 0 1 2	EXPONENT 0 1 2	EXPONENT 0 1 2	EXPONENT 0 1 2

77	78	79	80
1/C=	1/C*	1/C•	1/C-
COEFFICIENT -2.8240400E-01 1.0108175E+00 -4.7151498E-05	CUEFF LCIENT -3.3900080E-01 1.0117118E+00 -4.8660568E-05	COEFFICIENT -3.2247594E-01 1.0114324E+00 -4.8182073E-05	COEFFICIENT -2.6107879E-01 1.0098416E+00 -4.0564349E-05
EXPONENT 0 1 2	EXPONENT 0 1 2	EXPONENT 0 1 2	EXPONENT 0 1 2

APPENDIX C

PROGRAM LISTING

```
- MERSIAN OS LULY 1983
- MTHIS IS A MODIFICATION OF A PROGRAM ARITTEN BY A. HANNIARACHCHI FOR GENER
E ON THE HADOSH
. .
 ١,
AL USE ON THE HEAD STATE OF STATE MODIFICATIONS DONE BY H. KEEBLER FOR TESTING ON THE THE STATE ACQUISITION SYSTEM. MODIFICATIONS DONE BY H. KEEBLER FOR TESTING ON THE
                1 004

104 (0. 4039),E(39),0(19),0(7)

DIM Em+(39),T(39),En+1(39)

HSSIGN #Coe TQ "CDE"

FOR I=0 TQ 39

ENTER #Coe:A(I).B(I).U(I)
40
5912334
                MEX: 1
DATA 0.10086091.25727.94369.5727345.0295.79025595.81
DATA -9247486589.6.976886+11.-2.661926+13.0.940796+14
READ 0(*)
95
105
110
                BEET
PRINTER IS 701
CLEAR 709
INPUT "ENTER RESISTOR VOLTAGE".RV
INPUT "ENTER LOAD VOLTAGE".LV
130
                 4mp=44/2.3
               Amp.*
Amp.*
Pow*Amp*Lo
PRINT "RESISTOR VOLTAGE=".Rv."*/NLTS"

PRINT "LOAD VOLTAGE= ".Lv."*/DLTS"

PRINT "CURRENT= ".Amp."*Amp."*
PRINT "PUMER= ".Phw."*MATTO"

INPUT "ENTER MONTH.DATE, AND FIME (MM:DD:HH:MM:GS)",FimeS
OUTPUT 709:"TD";FimeS
PEED
136
137
138
139
              BEEP TOSAGE AUTO, 2-FILE, 3-MANUAL)". In

REEP TOSAGE THEN

REEP TOSAGE TO SAGE FROM DATA FILE". TOAT TOLD THESE RESULTS ARE FROM DATA FILE". TOAT TOLD THESE END IF

IF IMPTOR IN-3 THEN

REEP TORAGE TO SAGE THEN

REEP TORAGE TO SAGE THEN
160
190
190
200
210
220
230
240
              BEEP
THEN DATA FILE NAMED". Newfile'S CREATE BOAT Newfile'S. 30
ASSIGN SFILE TO Newfile'S INPUT "Enter number of Samples". It INPUT "ENTER WAIT TIME IN USC". I time END IF BEEP James
250
250
250
250
250
250
250
292
230
300
                GUTPUT 709:"AR AFAN AL79"
DUTPUT 702:"F1 R1 T1 Z1 FL1"
310
330
340
350
350
361
362
                J=U+1

IF Im=: OR Im=? THEY
*READ TEMP OF BOX WALL(INSIDE)
PRINT " "
                PRINT "INGIDE BOX WHEN TEMP"
354
               PRINT "INSIDE BOX #ALL IL"
FOR !=0 10 9
OUTPUT 709:"AS SA"
ENTER 722:Emf(!)
IF [<4 THEN 400
IF [>5 THEN 400
IF Emf(!)<.UU0001 THEN 400
370
320
390
 392
```

```
197
  399
  4111)
401
410
  429
  430
  340
  44 :
  442
  443
  444
                                                                            | T(1)+FMTemc(t,1)
| DRINT T(0).1+4',3
| NEXT | PRINT T(0).1+4',3
| PRINT ""
| PRINT ""ULM GI,GTI,GTO-EPROM/CHIP"
| IFOR ACTUAL
| FOR 1-12 TO 19
| OUTPUT TOQ TAS SA"
| ENTER 722:Enr(1)
| IF Emf(1).60001 THEN 464
| CALL TURVIENT(1).Enr(1))
| TI+Emf(1)
| I(1)+FMTemc(t,1)
| PRINT "I/O MODEL G2.G1,G10.G11.G12.G13"
| TREAD I/O BOARD TEMP
| FOR 1+40 TO 10
| OUTPUT TOQ TOS SA"
| ENTER 722:Enr(1)
| IF Emf(1)
| IF Emf(1)
| TURN TOO TOOM THEN SON CALL TURN COOL THE COOL THE
    445
  150
  45
452
454
455
455
457
    452
    254
    450
461
462
    465
  467
  47:j
480
    4.40
    491
    437
    493
                                                                                           PRINT TO LIVE
    4-4
    435
                                                                                         MEXI I
  580
501
                                                                                    PRINT"""
PRINT"""
PRINT"""
PRINT"""
PRINT"""
PRINT"""
PRINT"""
PRINT"""
PRINT""
PRINT""
PRINT""
PRINT""
PRINT""
PRINT""
PRINT""
PRINT""
PRINT"
PRINTT
       ša,
  510
520
530
540
       541
       543
         543
         . 44
         545
       550
551
552
                                                                                      PRINT "EXTERNAL BOX TEMP"
!READ OUTSIDE BOX TEMP
FOR I 48 TO "9
OUTPUT 709:"85 SA"
ENTER 722:Fm+(1)
IF Em+(1)<.00001 THEN 565
CALL Ivsv(Emf(1).Enf1(1))
            554
```

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```
MODEL
VERSION 13 AUG 1983
MINISTER A MODIFICATION OF A PROGRAM WRITTEN BY A. WANNIARACHCHI FOR GENER
ON THE HP3054
MINISTER ACCURATION SYSTEM.MODIFICATIONS DONE BY H. KEEBLER FOR TESTING ON
  .0
 20
  AL USE ON
  30
     THE
                   ! ULM
COM /Co/ A(39),B(39),C(29),D(7)
DIM Em((29),I(39),Emf1(39)
ASSIGN *Loe IO "COE"
FOR I=0 ID 39
 40
  50
  60
91
92
93
                    CI), CI) B(I), B(I), EVIER PCOE; A(I), B(I), C(I)
                    NEXT
                    DATA 0.10086091,25727.94369,-767045.2295.78025595.81
DATA -9247486589.6.97688E+11,-2.66192E+13.3.94078E+14
  95
105
                    READ D(=)
  110
                   BEEP
PRINTER IS 701
CLEAR 709
INPUT "ENTER RESISTOR VOLTAGE",RV
INPUT "ENTER LOAD VOLTAGE",LV
Amp=RV/2.0
  131
132
133
                   Amp=Rv/2.0

Fow=Mno=Lv
PRINT " MODEL OF ULM "

PRINT "RESISTOR VOLTAGE=".Rv."VOLTS"

PRINT "LOAD JOLTAGE= ".Lv."VOLTS"

PRINT "CURRENT= ".Amp."AMPS"

PRINT "POWER= ".Pow."HATTS"

INPUT "ENTER MONTH.DATE, AND TIME (MM:DD:HH:MM:SS)",Time$

GUTPUT 709:"ID";Time$

REF®
   134
125
137
138
   148
   141
                   INPUT "ENTER INPUT MODE(1-3054A-AUTO,2-FILE,3-MANUAL)", In IF Im-2 THEN REEP
  150
150
170
   98
                    TNPUT "SMIER NAME OF EXISTING DATA FILE".Oldfile$
PRINT USING "10%.""THESE RESULTS ARE FRUM DATA FILE"".10A":Oldfile$
ASSIGN **:le TO Oldfile$
  ASSIGN *File TO Didfiles
END IF
IF lm=1 OR Im=3 THEN
BEED
INPUT "NEW DATA FILE NAME?" Newfiles
CREATE BDAY Newfiles 40
ASSIGN *File TO Newfiles
INPUT "enter number of samples" It
INPUT "ENTER WAIT TIME IN SEC", I_time
END IF
BEED
1=0
  281
282
290
   300
  310
330
340
                  J=0
DUTPUT 709:"AR AF40 AL79"
OUTPUT 722:"F' R1 T1 Z1 FL'"
J=J+1
IF Im=1 3R Im=3 THEN
'READ TEMP OF BOX HALL (INSIDE)
PRINT ""
PRINT "INSIDE BOX HALL TEMP(45,46)"
PRINT "CPU-U3,BOARD(BOT/TOP)"
FOR I=0 TO 9
OUTPUT 709:"AS SA"
ENTER 722:Lmf(I)
    350
   360
  362
384
  365
370
380
```

```
IF Emf(I) <.00001 THEN 402

CALL Twov(Emf(I),Emf1(I))

It=Emf1(I)

IT I=FMTem(Tt.I)

IF I=5 THEN T(I)=0.

IF I=5 THEN 402

PRINT T(I),I+41,J

NEXT I

PRINT "INTERNAL AIR TEMP/AMBIENT(53)"

TREAD AIR TEMP MODEL

FOR I=10 TO 12

001PUT 709:"AS SA"

ENTER 722:Emf(I)

IF Emf(I) <.0001 THEN 450

CALL Twov(Emf(I),Emf1(I))

Tt=Emf1(I)

PRINT T(I),I+41,J

NEXT I

PRINT ""
 394
 395
396
397
   398
 400
401
 403
 410
420
 440
 441
 442
 444
                                                              PRINT T(I),I+41,J
NEXT I
PRINT " "
! PRINT "ULM U1,U11,U13-EPROM/CHIP"
!FDR ACTUAL
FOR I+13 TO 19
OUTPUT 709:"AS SA"
EMTER 722:Emf(I)
IF Emf(I)<.00001 THEN 464
CALL Tvov(Emf(I).Emf1(I))
It=Emf1(I)
! T(I)=FNTem(Tt.I)
! PRINT I(I).I+41.J
 445
 450
 452
454
   455
 456
457
458
 459
 469
                                                      ! T(!)=FNTem(Tt.!)
! PRINT T(!).!+41.J
NEXT:
PRINT ""
PRINT "!"
ENGL !/O 31

OUTPUT 709:"AS SA"
ENTER 722:Emf(!)
If Enf(!)<.00001 THEN 500

CALL 'vsv(Emf(!).Enf(!))
It=Enf(!)<.00001 THEN 500

CALL 'vsv(Emf(!).Enf(!))
PRINT "(!).!+4*,J
NEXT !
PRINT " ULM US. INTERNAL AIR"
**READ ACT BOARD TEMP
FOR I=52 TO 37

OUTPUT 709:"AS SA"
ENTER 722:Enf(!)
IF Emf(!)<.00001 THEN 550

CALL Tvsv(Emf(!).Emf(!))
IT=Emf(!)

**PRINT T(!).Emf(!)

**PRINT T(!).!+4!.J
NEXT !
T+=Emf(!)
PRINT T(!).!+4!.J
NEXT !
PRINT T(!)
PRINT T(!).!+4!.J
NEXT !
PRINT T(
   461
                                                                     ! T(I)==Niems: t.;;
! PRINT T(I).I+41.J
   462
 464
465
466
467
470
 480
491
 493
 495
 500
 501
502
510
520
530
 540
541
 542
   543
544
545
510
551
552
555
556
557
```

```
TreEn+*(1)
(1) = FNTen(Tr.1)

PRINT T(1) | 1+41 |
NEXT 1
QUIPUT #File:En+(+)
ÉLSE
ENTER BFile:Emi(*)
                                                 END IF
END IF
PRINT " "
PRINT "GMRIENT AIR+ ",T(J6),"77"
PRINT "SUMMARY"
  540
 500
500
501
610
550
                                                   Inax=0
IF Im=1 OR Im=3 ImEN
                                               The stage of the s
  570
    6.21
(10)
    63.)
493
       305
     596
- 18
       700
        703
705
706
        707
                                                         END
SUB TVEY(V.T)
COM (Co/ AC39).8(39).C(39).D(7)
                                                        CUM /CO/ AC397.8
Sum=9
FOR [=0 TO T
Cum+Sum+B(I)=V [
NEXT ]
            7-0
7-1
                                                      NEXT T
T+(Sum=9/5)+32
SIBEND
+THIS FUNCTION HISES CALIBRATION COEFICIENTS
+TO ADJUST THERMOCUUPLE READINGS
DEF FNIen(T.1)
COM /Co/ A(29), P(29), C(29), D(7)
Delta=A(1)+(+(B(1)+T+((1)))
T+T+(Delta
RETURN T
FNEND
         780
730
           ลบก
เปล
           820
310
            840
              350
            850
370
```

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APPENDIX D

ULM DATA RUN 1 AUG 83

- A. LOCATION: Root Hall, Room 107
- B. CONDITIONS:
 - 1. Backpack placed in the environmental chamber in a vertical position.
 - 2. Initial temperature: 48.3C
- C. CONDUCT OF RUN:
 - Part I 8 samples were taken at 5 minute intervals.

Initial electrical readings were as follows:

resistor voltage = 3.053 load voltage = 5.3 current (amps) = 1.53 power (watts) = 8.09

2. Part II - 20 samples were taken at 30 minute intervals. Electrical readings (same as settings as part I) were as follows:

> resistor voltage = 2.88 load voltage = 5.27 current (amps) = 1.44 power (watts) = 7.59

THIS	DATA IS	FROM	1 AUG 83	-ULM		
TIME(MIN)	TC=	53	TC=	54	TC-	55
0 5150 50 12250 330 100 100 100 100 100 100 100 100 10	47.8419 50.0519 51.9584 53.3484 53.3484 55.59343 55.59343 57.7460 56.5479 58.2656 59.84:45 60.2289 60.2289 60.2289 60.23665 60.23665 60.5799 60.7665 60.7665 60.7665 60.7665	163325 254154 079445 2794473 771337 257794 721356 3721	47.954495 50.14495 60.14495 60	632526 375838 199174 730048 415172 698769 181363 698769 181363 1217706 3017726 23017726 2301776 825744 943776 825777 9243776 8257777 9267777 9267777 92778 9	55.14297 60.24766297 60.5496297 60.549681401 60.549687567 60.549687567 60.549687567 60.549687567 60.549687567 60.549687767 60.549687767 60.56967	7689945956815+340994457-425294596577+200564650994457-425294667926445492974457929449229449229449229449229449229449229449229492294922949929499294992949929499294992949929499294992949929499294992949929499294992949929499

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TIME (MIN)	TC=	5 6	TC=	57	TC=	58
0515050334700000000000000000000000000000000	59.2646 64.75689 68.8606 70.8941 71.5884 72.1238 73.1031 74.6882 75.0963 76.2287 76.3363 76.3363 76.3363 76.363 76.6897 76.6897 76.687 76.8518 76.8587	593407 145273 82052 82052 82052 870788 1777223 1777223 142752468 157964086 1579649 157964 157964 157964 157964 157964 157964 157964 157964 1604 1604 1724 1724 1724 1724 1724 1724 1724 172	62.7103 66.4822 68.5173 69.8221 70.7684 71.0541 72.0531 74.1944 74.6418 75.9941 76.2057 76.4077 76.3539 76.4077 76.5690 76.5690	9772 1577964 4230911 8408179 1004269 1389563 4448021 8138627 8138622 8137546 8177546 81775161	53.67418 61.96567 67.57265 67.57265 68.77265 68.77265 70.50501 71.06351 72.03680 73.63640 73.18165 74.785140 75.18731 75.18731 75.32645 75.32645 75.32645 75.56278 75.56278 75.68984 75.68984 75.79268	993516 993516 993516 993516 993516 993516 9936 9936 9936 9936 9936 9936 9936 99
_						

TIME (MIN)	TC=	59	TC=	50	iC=	73
0 10 10 15 20 30 30 10 10 10 10 10 10 10 10 10 10 10 10 10	71.5466 71.603 71.675 71.729 71.772	371873 306303 340167 777772 732575 981594 981594 983118 983159 983159 984536 984536 98664376 9890053	59.748 62.748 62.748 64.6516 65.243 67.768 69.376 71.368 71.368 71.368 71.71.997 71.997 71.997 71.997 71.997 71.997	5719066 1540954 7069186 4793469 9793459 9795521 9795521 979785 979795 9797979 97979 97979 97979 97979 97979 97979 97979 97979 97979 97979	78.3200	40000400000000000000000000000000000000

TIME(MIN)	TC=	74	TC=	75	TC=	76
05150 1150 12233340 1030	57.7635 64.23185 66.71863 69.8959 70.99360 71.8969 72.3586 74.8597 74.86945 75.0338 75.0388 75.0388 75.1874 75.4669 75.3566 75.3566 75.3566	309951 211319 211319 2249777 3059733 3147097 5168594 5168594 51795617 5139085 51795617 517972 51773972 51773976 51773976 5177508 51775	53.315 55.55325 55.553.59 57.5339 59.4951 59.4951 59.4951 59.4951 69.2922 69.2933 69.3933 6	0231928 27:9992 92:446 93:176 6033272 5064257 87:254 64:6153 0657903 9488273 7106844 7243:545 6568004 5852891 270055 7727052 9748809	49.939999999999999999999999999999999999	97.44.003.79.74.003.79.28.14.6956.97.44.003.79.69.79.69.79.69.69.69.65.67.8956.67.8956.67.8956.67.8956

TIME (MIN)	1.C =	77	ĭC=	78	TC=	?3
0 5 10 15 20 25 30 35 40 70 130 130 190 2250 280 340 340 340 460 490 5550 580	48.0503 48.1074 48.1309 48.1262 48.1427 48.1333 48.1427 48.1351 48.12156 48.21815 48.2	555193 7018742 7018742 7018742 841836 841836 811456 991935476 991935476 991935476 991935476 991935476 991935476 991935476 991935476 991936	47.38991 48.38991 48.38991 51.38999 51.389999 51.389999 51.389999 51.389999 51.389999 51.389999 51.389999 51.389999 51.3899 51.3899 51	4507086 7198125 9955848 1718085 7208867 7465453 8415058 8119746 8415058 8119746 8415058 8119746 8415058 8119746 8415059 81176374 93894726 83894726 83894726 83894726 83894726 83894726 83894769	47.98658 47.98658 48.03568 48.0114578 48.0114578 48.11620255 48.11620255 48.1220551116 48.223651116 48.223651116 48.22642 48.23661116 48.22642 48.2142 48.2142 48.32642 48.32642 48.32642 48.32664 48.326	225699138847 4444926 7556884492691388479 75688449926913888479 75768884150875807 7576888479 7576888479 7576888877 75768888 75768888 7576888 7576888 757688 757688 75768 7
610	48.6033	548485	55.9210	1305/1	48.71350	162333

TIMECHIN	TC =	80	TC=	72	TC=	71
0 10 15 25 35 40 10 10 10 10 10 10 10 10 10 10 10 10 10	47.7538 48.17538 48.77468 49.27665 50.6668 50.6668 51.6688 52.31768 52.31768 53.42177 53.42177 53.42177 53.42177 53.42177 53.6245 53.42177 53.6245 53.42177 53.6245 53.6527 53.6527 53.89974 899748	718775 8807575 8807575 880775 880379 8421636 8412876 841287770 841287770 841287770 841288 841288 841288 8412	46.69733 48.152316 48.152316 48.152317 48.152317 48.152317 497.365467 727.77 497.365467 727.77 497.318482 509.5000 497.32784 497.32784 499.5000 499.5000 499.5000 499.5000 499.6000 499	434802 92051 92051 920551 920551 920551 926551 926552 926562 926562 926562 926562 926562 92752	7.06020000000000000000000000000000000000	**************************************
			3		2.12000	

APPENDIX E

ULM DATA RUN 12 AUG 83

A. LOCATION: Ft. Hunter Liggett Ca.

B. CONDITIONS:

- 1. The backpack was placed on a concrete slab outside in direct sunlight in an upright position.
- 2. Initial temperature: 23.8 deg C

C. CONDUCT OF RUN:

1. Part I - 10 samples were taken at 3 minute intervals. Initial electrical setting was at zero to check the effect of solar radiation on the internal temperature of the backpack.

resistor voltage = 0.0 load voltage = 0.0 current (amps) = 0.0 power (watts) = 0.0

2. Part II - 15 samples were taken at 5 minute intervals. Electrical readings were as follows:

> resistor voltage = 3.05 load voltage = 5.21 current (amps) = 1.52 power (watts) = 7.93

3. Part III - 10 samples were taken at 15 minute
intervals. Electrical readings (w/same setting
as part II) were as follows:

resistor voltage = 2.86 load voltage = 5.29 current (amps) = 1.43 power (watts) = 7.56 4. Part IV - 8 samples were taken at 15 minute intervals. Orientation was changed to maintain the direct nature of the sun's rays. This caused the backpack to be moved to a position on dirt rather than the concrete slab. Electrical readings (w/same setting as part II were as follows:

resistor voltage = 2.82 load voltage = 5.28 current (amps) = 1.41 power (watts) = 7.44

THIS	DATA IS	FROM	12 AUG 8	33 -ULM		e
TIMECHIND	TC=	53	TC=	54	rc=	55
036911122234455566778889910550505050505050505050505050505050505	24.77.6865.66.27.4988.65.66.27.74886.56.66.27.77.6866.56.66.27.6866.56.66.27.68.27.28.28.28.28.28.28.28.28.28.28.28.28.28.	35107847953128999533368242926944444333210784547953128999537253489953242795547953128999533368224279555514484444444444444444444444444444444	31.626668 1.96586668 1.96586668 1.96586668 1.96586668 1.96586668 1.9658668 1.9658668 1.9658669 1.965869	28-28-28-28-28-28-28-28-28-28-28-28-28-2	40000000000000000000000000000000000000	# 22 * 1 * 1 * 1 * 1 * 1 * 1 * 1 * 1 * 1

TIME(MIN)	TC=	56	TC=	57	TC=	58
035911814750505050505050505050505050505050505050	66.0973 66.09454 67.8106 68.6380 69.4485 70.20430 72.12579 74.4893 74.4993 74.49631 75.4964 75.954 77.1017 78.306 78.435	553739 00270367 00270367 00270367 00270367 0031894 400457 400457 400457 400457 400457 400457 400457 400457 400457 40045	25.033 036 036 036 036 036 036 036 036 036	76034569 7034569 7034566 7034566 7034566 703456 703456 703456 70356 70356 70356 70356 7036	29.6324 30.5100 30.5264 30.5264 31.0000 31.000 31.000 31.000 31.000 31.000 31.000 31.000 31.000 31.0	40000000000000000000000000000000000000

TIME(MIN)	TC=	59	TC=	60	TC=	72
036911814750505050505050505050505050505050505050	31.0018 31.7694 32.5238 40.4641 47.0581 50.7180 53.1936 55.0751 56.6630 59.2766 60.3348 61.2209 62.9666 62.9666 62.9666 62.7909 65.3777 66.9441 67.3176	7133702 713370	47.7034 51.3701 53.72105 55.3105 57.3105 59.9524 612.55749 612.557	9600643943942459525137251439712271365553795143971222713659595	23.5200500500970540050002440050005000500050005000500050	9454973672:07255669456:00:07094786044039998:04749245686:7599557995:00:03995:70:35969:70:3995:7

0 24.5643553789 25.0330727016 25.199913 3 25.5643553789 26.0232867812 26.169865 6 26.555008818 26.0232867812 27.098748 9 27.4696027387 26.9698790575 27.098748 12 29.342360367 27.863221385 27.384354 15 29.2010203296 28.730750649 29.841556 18 30.0498741694 29.5820334967 29.592420 21 30.870540251 30.4052095331 30.510256 24 31.6558704294 31.202709006 31.300056 27 32.415734675 31.9771313647 32.05572 35 46.9613425352 41.533891534 40.025372 40 52.7393840739 50.2132710082 47.81643 40 52.7393840739 54.56866447556 51.78253 45 55.8720955705 54.56866447556 51.78253 50 58.1483921073 57.2607604905 58.22415 50 59.9661207607 59.2276681289 57.81720 50 60 61.5596594548 60.3589280992 57.81720	TC* 58
76 64.1644.727 75 65.2205181273 54.6153497197 61.48650 80 66.0973001624 65.5039784161 62.39101 80 66.0973001624 65.5039784161 63.22996 85 66.9454827956 56.3562693677 63.22996 90 67.8106023861 67.2154431938 64.10201 95 68.6380954314 68.0454897168 54.94535 100 69.448539572 68.8562080605 55.74870 105 70.2012052456 69.6136802267 66.52133 105 70.3488500007 70.2795355754 57.18374 115 70.3488500007 70.2795355754 57.18374 115 70.34885000007 70.2796363 58.44077 130 72.1103477099 71.5799253869 58.44077 145 73.2564637567 72.7027799663 59.56543 145 73.9795372136 73.4630912407 70.28713 160 73.9795372136 73.4630912407 70.98948 175 74.4723420531 73.9695089315 70.79678 190 74.5892948029 74.0954835201 70.88948 190 74.6679899923 74.0954835201 70.89948 205 74.4993232902 74.0954835201 70.89948 205 75.4859146318 74.999425514 71.37980 220 74.6679899923 74.4995278791 71.37980 235 75.9640956691 75.5557375665 72.69063 250 75.4859146318 74.9945257862 72.99093 265 75.9640966891 75.5557375665 72.69063 295 76.5201735935 76.716887639 73.77168 295 76.5201735935 76.716887639 73.77168 295 78.0179382599 77.5910592326 74.8932 340 78.3062522779 77.87131136446 74.8932 340 78.3062522779 77.87131136446 74.8932	28.8415560765 29.6924286795 30.65102560765 31.3000588139 32.0571201752 47.815438752 47.815438752 47.8255697467 31.78255697467 31.78255697467 31.78255697467 31.78255697467 31.78253697467 31.78253697467 31.78265697467 31.782656979 31.782656979 31.7826779 31.7826779 31.782669 31.7826699 31.7826699 31.7826699 31.7826699 31.7826699 31.7826699 31.7826699 31.7826699 31.7826699 31.7826699 31.7826699 31.7826699 31.7826699 31.7826699 31.7826699 31.7826699 31.7826699 31.7826699

TIME(MIN)	TC=	73	TC=	74	T	C=	75
0369115814750505050505050505050505050505050505050	24.623 25.6240 26.5240 27.4070 28.2616 29.9127 29.9124 31.1909 31.4618 47.9599 47.4784 47.4784 57.4786 65.9829 65.9829 65.9829 65.9829 65.9829 67.4831 67.4926 68.4892 68.4892 68.4892 68.4892 68.4892 68.4892 68.4892 68.4892 68.4892 68.4892 68.4892 68.4892 68.4892 68.5292 77.6606 77.6606 77.6606 77.6606 77.6606 77.6606 77.6606 77.6606 77.6606 77.6606 77.6606 77.6606 77.77.6606 77.6	548555 5476585 5476585 5476585 5476585 547859866555 5477459866555 547859866555 54775986655 54775986655 548959465 54895986655 54895	54.1556 56.1770 56.1770 57.2371 59.56440 61.66440 62.6440 63.415684 65.751441 60.4568 67.11.6640 67.11.6640 771.6928	2681727 27252424 27252424 271752424 21752424 21752424 21752424 21752424 21752424 2175242 217524 217	567990125005689026456678001-111-120064555 202223666666666666666666666666666666666	750539 744245 7444923 6499886 4499886 444923 77134493 77134493 772276584 653428 4928	4411 4 6+797 64 631957 404 5696 86990009 411 687 47956 8696 4096 8696 8696 8696 8696 8696 8696 8696 8

TIME(MIN)	TC=	76	IC=	77	TC.	73
036911514750505050505050505050505050505050505050	25.733617 26.733617 26.733617 27.64617 27.64617 27.64617 27.64617 27.64617 27.64617 27.64617 27.64617 27.6617	994544 994546 994546 994546 994546 994546 994546 994546 99456 9956	42.458827742882774288277428827742882774288277428837774288377446.093774866478447864784478647833235553235553335553335553335553355533	00580580514285 100580714285 100580714285 100580714285 100580714285 100580714285 100981487807 100981487805 100981487807 10098148828808478678688888888888888888888888888888	27.75547 27.75547 27.75547 27.75547 27.75547 27.75547 27.5559 27.6559	0.871-87042254848498549944967475949495956825174769544869449854994959548486944969447695784486944969449695476957697844969944969769576976976957696779877695974969674877696779867799676956877456974959687496959687459596874959687495968749596874959687495968749596874959687495968745959687495968749596874959687495968749596874959687495968749596874596874959687596874969687496896896896896896896989689698968969896896

THIS	DATA IS	FROM	12 AUG 8	3		
TIME (MIN)	TC=	79	TC=	80	TC=	53
036911814750505050505050550505050505050505050505	52.9245 54.0417 54.4725 54.7356 54.76517 54.75517 55.3356 55.6513 57.1783 57.1783 57.4698 60.1502 58.953	037018 0301803 0301803 0301803 0301803 0412829 0412	52.0431 52.3419	094972 7849742 7849742 78578 78578 78578 78578 78578 78578 78578 78578 78578 78578 78578 78578 78578 78578 7858 78578	58.711364 59.244883 59.339523	0 988 57647950 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0

APPENDIX F

MODEL DATA RUN 15 AUG 1983 (48.8C AMBIENT)

- A. LOCATION: Root Hall, Room 107
- B. CONDITIONS:
 - 1. Backpack placed in the environmental chamber in a vertical position.
 - 2. ambient temperature: 48.8C
- C. CONDUCT OF RUN:

Part I - 8 samples were taken at 5 minute intervals.

Initial electrical readings were as follows:

resistor voltage = 3.06 load voltage = 5.17 current (amps) = 1.53 power (watts) = 7.91

Part II - 20 samples were taken at 15 minute intervals.

Electrical readings (same settings as part I) were:

resistor voltage = 3.1 load voltage = 5.40 current (amps) = 1.55 power (watts) = 7.97

DATA IS F	RCM	15 AUG 83	3 -MODEL		
TC=	41	TC=	42	TC=	43
52.62926 57.095:0 57.76020 57.76020 57.769544 59.58499 60.4959:0 61.850177 61.4798131 62.659177 53.705330 70.21698 54.27256	96768 79766 79766 5976234 5976234 5923453 592356 59236 592356 59236	52.97400 52.97400 55.97400 57.29604 57.29604 57.29605 61.17206 61.17206 62.7566 63.446 63.446 63.446 63.446 63.4766 63.446 63.446 63.666 63.666 63.666 63.666 63.666 63.666 63.666 63.666 63.666 63.666 63.666 63.666 63.666 63.66	527849 462609 111824 111824 1118234 1118234 111837334 111837337334 111837334 111837334 111837334 111837334 1118374 1118374 11	48.240924 50.7024790 52.546790 53.8224700 53.8224700 53.8224700 557.0245440 557.0245440 557.0245440 557.0245440 557.0245440 577.0245440 577.0245440 577.0245440 577.0245440 598.7864 598.7866 50.9852374	528469306975042257535317494649467060135727674747467288756017572767676387288728872887288728872887288
				61.539276	9203
	48.04234 52.62926 57.09510 57.760544 59.58417 59.58417 61.478 61.478 62.65917 57.69345 62.65917 53.726936 62.209420 63.21699 64.2725 55.22427 54.52427 54.52393 54.52393	TC* 41 48.0423417034 52.6292696768 57.0951079766 57.7603061225 57.6954432734 59.5849958463 60.4617159658 61.8501662293 60.4017729355 61.4797830763 62.659112520 57.2017779454 53.6942527516 56.7030382915 70.2584562907 54.2189880976 54.2725999077 64.8356645255 54.3611646605 64.9624809237 64.9734919472 65.0471055759 54.5033050237 54.5293330428 54.5242734904 54.5662080626	TC= 41 TC= 48.0423417034 48.26176 52.6292696768 52.6408 57.0951079766 55.9724 57.7603061025 57.9745 57.6954432734 59.29604 59.58449958463 60.29445 60.4017159658 61.07916 61.4797830769 62.0495 61.4797830769 62.0495 61.4797830769 63.1051 62.1881324611 53.79476 62.659112520 64.2365 57.2017779454 64.6825 57.2017779454 64.6825 57.2017779454 65.4274 53.6942527516 64.6825 56.7030381804 55.4274 55.2633082915 65.9751 70.2584562937 55.98656 54.2725999077 56.2276 54.3654646605 66.37626 54.9784919472 56.44374 54.5299330428 56.44312 54.5299330428 56.46315	TC* 41 TC* 42 48.0423417034 48.2617698275 52.6292696768 52.6408527849 57.0951079766 55.9724462609 57.7603061025 57.9745111823 57.6954432734 59.2960903914 59.5849958463 60.294489838 60.4617159658 61.07953712 61.8501662293 61.7210520301 60.4017729355 62.0495808733 61.4797830763 63.1051192634 62.1381324611 63.7947659092 62.659112520 64.2365346108 57.2017779454 64.6825387371 56.7030081804 65.427402323 55.2633082915 65.9751532211 70.2584562907 66.1735999502 54.2169880976 66.1735999502 54.2762060998 66.2762060998 54.361464605 66.3651220236 64.9624809237 66.4107146747 64.9784919472 66.4357891136 65.0471055759 66.449465626 54.5033050237 66.4312302049 54.5299330428 56.4631418177	TC+ 41 TC= 42 TC= 48.0423417034

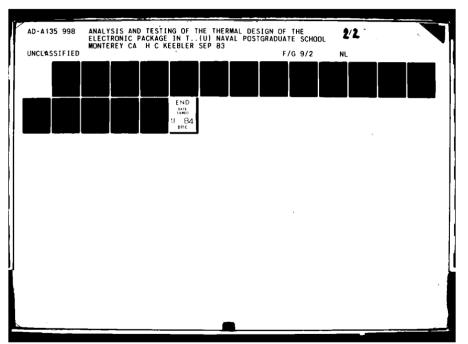
Reproduced from best available copy.

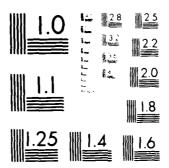
TIME (MIN)	TC=	53	· TC=	79	1	ĩC∗	30
051505050505050505050505050505050505050	47.9736 48.0207 48.11020 48.1550 48.1550 48.2928 48.3506 48.4257 48.57386 48.4257 48.73256 48.89385 48.99556 48.99526	724131 724131 722913 722903 92903 9476591 950225 75081 749525 749525 166597 959049 9590499 947748 870788 870788	48888888888888888888888888888888888888	108624967 155721324 221649445 221649445 221649445 23163818762 3534813762 373496131 373496131 373496131 373496131 373467637 373467637 373467637 373467637 373467637 373467637 373467637 373467637 373467637 373467637 373467637 373467637 373467637 373467637 373467637	48900:111233333444444444444444444444444444444	.927563 3.91773 3.912925 3.5320777 .128429 3.5320777 .128429 3.65273 .40922 .475932 .475932 .475932 .475932 .475932 .2475932 .2475932 .2475932 .234279 .234279 .234279 .234279 .23428 .23428 .24	9575+6387888+62595+84+5566666575+64557888+67884580877889
		0.2.00	70	03715173	, , ,	.497974	0103

TIME (MIN)	TC=	44	TC=	45	TC=	45
0 5 10 15 20 35 40 50 85 85 10 10 10 10 10 10 10 10 10 10 10 10 10	48.2174 51.0609 53.396 53.3781 55.3863 56.3863 56.3863 57.4069 59.023 59.023 59.023 60.957 60.227 61.243 61.456 61.456 61.456 61.456	4110082 4488026 8993299 7095651 652914 652914 8059448 801259448 801259448 801259448 80125945 80125105 80125105 801257 8012545 801254	48.25287 48.25287 50.562583 50.5645607 52.3021607 52.3021607 53.322607 54.717556 6.89769 57.25567 57.2557 57.3078 57.	463971 463971 16423885 1333837 7564285 7564285 980041155 6404291 980041155 64044829 9104291 91044829 910	90 90 90 90 90 90 90 90 90 90 90 90 90 9	**************************************
310 325	61.5097 61.5764		57.3810 58.0481		62,51501 63,19312	

TIME (MIN)	TC=	47	TC=	48	TC=	4.3
0 5 10 15 20 35 40 57 85 10 10 10 10 10 10 10 10 10 10 10 10 10	48.79493 51.79493 51.79493 51.79493 51.79493 51.79493 51.79493 51.79493 51.79493 51.4433 51.	959205 006773 8375657 8847565 847565 8466647 4275666 955559 955559 977765 97766 97766 97766 97766 97766 97766 97766 97766 97766 9776 9776 9776 9776 9776 9776 9776 9776 9776 9776	48.0552 49.3242 51.3249 52.5209 53.1367 54.7789 55.608 57.8796 59.2576 59.2576 59.553473 59.56327	9853479 9853479 96135479 96135379 96135379 96135379 96135379 9613537 9613537 9613537 961353 961353 96135 961	48.67.062.06.06.07.06.06.07.06.06.06.06.06.06.06.06.06.06.06.06.06.	#48613

* C =	50	IC=	51	IC=	52
47.9679 49.1459 50.5534 51.7845 51.78379 53.6773 54.38379 55.27739 54.38379 55.27739 57.8694 57.8694 57.8694 58.7224 58.7224 58.7224 58.7224 58.7224 58.8218 58.8218 58.8218 58.9211	252179 026629 752299 352736 1274447 421447 4214468 5079605 555404 7710221 452745 603344 603342 603342 603342 603342 603342 603357	48.55.56.44.55.56.45.56.45.56.45.56.45.56.56.45.56.56.45.56.56.76.56.56.76.76.76.76.76.76.76.76.76.76.76.76.76	100 100 100 100 100 100 100 100 100 100	50.986234 59.82234 59.82234 66.02663 66.47453 66.47453 66.39763 67.1.37923 67.1.37923 67.1.37923 67.1.37923 77.1.39968 77.1.39968 77.7223 77.733 77.7	135,436,6 135,436,6 135,436,6 137,135,4 137,13
	47.9679 49.1459 50.55345 51.78379 53.6773 54.9673 54.9673 55.2773 54.9673 55.2773 56.9374 55.2773 57.6864 57.8693 57.8693 58.72549 58.72549 58.72549 58.8059 5	TC= 50 47.9679052179 49.1459026629 50.5504782299 51.7845362736 52.8379127414 53.6773016447 54.38287420015 54.9643421461 55.27.1180488 56.2739505896 56.3253079605 57.6392982934 57.8604771022 58.0593503321 58.339043296 58.7254603328	47.9678052179 49.1459026629 50.5504782299 51.7845362736 52.8379127414 53.6773216447 54.3828742001 54.9643421461 59.08742 55.271130488 55.271130488 56.2739505896 56.3253079605 56.3253079605 57.6892982934 57.6892982934 57.6892982934 57.8604771022 58.0593503321 58.339043296 58.3593503321 58.339043296 58.7225327745 58.339043296 58.72594603328 58.7254603328 58.7254603328 58.7254603328 58.7254603328 58.7254603328 58.7254603328 58.7254603328 58.7254603328 58.72548603749 58.7254603328 58.72548603749 58.72548603749 58.72548603749 58.8056667762 58.80593503308 58.72548603749 58.8056667762 58.80593503087 58.8058666778166 58.80586667849 58.80586667849 58.8058668207 58.805868207 58.8058668207 58.8058668207 58.8058668207 58.8058668207 58.8058668207 58.8058668207 58.8058668207 58.8058668207 58.8058668207 58.8058668207 58.8058668207 58.8058668207 58.8058668207 58.8058668207 58.8058668207 58.8058682007 58.8058682007 58.8058682007 58.8058682007 58.8058682007 58.8058682007 58.8058682007 58.8058682007 58.8058682007 58.8058682007 58.8058682007 58.80586820	47.9679252179 49.1459026629 50.5504782239 51.7845362736 52.8379127414 57.5745388631 53.6773216447 53.5351502121 54.3828742001 59.0874330607 54.9643421461 59.9943327911 55.271130468 60.2560142215 56.2739505896 61.3655898649 56.3253079605 62.5240981621 57.6892982934 57.8604771022 63.0682062731 58.339043296 64.4268388817712 58.7294603328	47.9679052179 48.6466056613 50.98664 49.1459026629 52.2153654553 59.82223 50.5504782239 54.9726603338 63.79234 51.7845362736 56.8413476409 66.02604 52.8379127414 57.5745388631 67.47603 53.6773316447 58.5851502121 58.51459 54.3828742001 59.0674330607 69.02215 54.9643421461 59.9943327911 69.8936 55.271130468 60.2560142215 70.17607 55.273130488 60.2560142215 70.17607 56.3253079605 61.3655898649 71.35216 57.3745655402 62.5240981521 72.17361 57.6892982334 52.3711251445 72.69223 57.8604771022 63.0682062731 72.49703 58.0593503321 63.5857971934 72.49703 58.339043296 64.03888171 73.42873 58.7294603328 64.3270239891 73.79784 58.7294603328 64.4298972372 73.89587 58.8218278166 54.508754866 73.389587 58.8218278166 54.508754866 73.39505 58





Microphy Resolution test chart-

TIME(MIN)	īC=	61	TC=	62	TC=	60
TIME (MIN) 0 5 10 15 20 25 30 35 40 55 70 85 100 115 1365 140 175 190 205	55.0174 67.3440 72.4016 74.7433 76.2636 77.2617 78.0406 78.5231 78.7359 79.5664 79.3163 80.4627 81.4866 78.0406 78.0406 81.03667 81.7967 81.7367 81.7367	063642 189924 785399 9785399 981403 501624 81905 129215 8205015 2228021 81905 404203 4746337	53.71.6 63.9949 68.2956 70.3751 71.7548 72.7028 73.4532 73.9539 74.1939 75.3668 75.3768 77.3012 77.3012	3444363 9034532 9034532 991324 8913247 8915964 902577364 902777364 90277364 90277364 90277364 90277364 90277364 90277366 902766 902766 902766 902766 902766 902766 902766 902766	58.9812 71.6422 75.4900 77.4437 79.7318 80.7995 80.7995 92.9500 83.4991 83.4991 83.6991 83.6991 84.258	990400501701454591909400170140001501701400015017014000150170140015017014001701501701400170150170140017015017014001701501701400170150170170170170170170170170170170170170170
220 235 250	91.7156 82.2467	243292	77 . 2542 77 . 7039 77 . 7396		34,2519 84,3448 94,3890	118197
250 265 290 295 310 325	82.2900 81.5688 82.2911 80.6275 82.4256 81.8401	97304 451771 547075 083994	77.1557 77.7799 76.4211 77.876	767701 9386657 414047	84.3779 84.4155 82.4290 84.3824 84.4575	800385 684833 172933 023303

TIME (MIN)	TC=	54	TC=	55	TC=	66
05 10 15 15 25 33 40 57 81 15 15 15 15 15 15 15 15 15 15 15 15 15	74.751- 74.8548 74.8975 74.8500 74.9402 74.1120 74.8950	(147329 19.47329 19.47325 19.5737 1	65.76246 73.5246 73.5246 85.53438 85.53438 87.7339 87.7339 88.010266 89.012	22107475 40757 40757 40757 40757 40759 407	59.766 77.766 77.77	5090640516 5090640516 5090640516 5090640516 5090640516 509066 50
325	74.555	110002	JL. 103	,,,,,,		

TIME (MIN)	TC=	67	TC=	63	TC=	69
TIME (MIN) 0 5 10 15 205 305 40 570 85 100 115 130 145 160 1750 2225	TC= 48.3491 48.5144 48.5147 48.51479 48.8189 48.9559 48.9559 48.9555225 49.22589 49.22589 49.22589 49.3337 49.3257 49.3257 49.49 49.49 49.49	146664 169617 12775647 12775647 7775644 209135409 48715609 48715609 48715609 48715603 48715603 48715603 48715603 48715 4	54.4364 50.3473 54.2174 65.1375 69.1814 70.5877 70.3877 71.3887 72.3887 73.4293 75.5507 75.5507 75.5507	9562752 952176 9087833 9196012 9996149 9497922 2297527 0402032 0402032 0402034 129034 1290404	48.556.584.65.475.45.05.756.475.45.05.755.45.05.755.66.66.66.66.66.66.66.66.66.66.66.66.6	. 450.4 65.4 96.7 4 47.4 57.4 50.4 7.4 60.4 60.4 60.4 60.4 60.4 60.4 60.4 60
250 255	49.4906 49.5288	611343	75.3020	201143 4484465	67.0467 67.0900	136607
290 295 310 325	49.5312 49.3152 49.3316 49.3316	*10308 643437 980309	76.0258 75.081	5288002 2125386 0715482	57.1151 67.0239 57.0553 67.1675	13657 443521 573 68

TIME (MIN)	TC=	70	IC =	71	r	C=	72
0 5 10 15 20 30 30 35 40 57 85 10 13 14 16 17 19 19 19 20 20 11 10 10 10 10 10 10 10 10 10 10 10 10	48.8654 55.1354 58.9676 61.5676 63.6672 64.5034 65.13677 66.2368 65.46774 67.7032 68.0625 68.0625 69.1752 69.45295 69.45295 69.5767 69.5767 69.5767	28116 28116 28116 283767 154116 777787 214775 214776 2477	48.0368 48.0840 48.1405 48.1405 48.1405 48.1224 48.22442 48.225 48.235 48.3303 48.3303 48.3303 48.4403 48.550 48	81375 81375 81249277 812492777 814937573 816493779 8164937 8164937 8174477 8174477 81849 81849 8	55. 65. 71. 72. 73. 75. 75. 76. 77. 77. 77. 77. 77. 77.	191055 191055 191055 191055 191055 191055 191055 191055 1910	430014759964459967 F7500 43014759074964450951 6490 43014759074960504450951
280 295 310	59.6809 69.4338 69.6084	603355 514366	49.5857 48.6021 48.6068	894745 969256	75. 77.	275417 949416 257513	57117 32373
325	69.6945	74:3/b	49.6304	202102	77.	349246	35 · 3

APPENDIX G

MODEL DATA RUN 15 AUG 1983 (37.7C AMBIENT)

- A. LOCATION: Root Hall, Room 107
- B. CONDITIONS:
 - 1. Backpack placed in the environmental chamber in a vertical position.
 - 2. ambient temperature: 48.8C
- C. CONDUCT OF RUN:

Part I - 15 samples were taken at 5 minute intervals.

Initial electrical readings were as follows:

resistor voltage = 3.27 load voltage = 4.72 current (amps) = 1.64 power (watts) = 7.72

Part II - 24 samples were taken at 30 minute intervals.

Electrical readings (same settings as part I) were:

resistor voltage = 2.8 load voltage = 4.73 current (amps) = 1.40 power (watts) = 6.62

THIS	DATA IS F	ROM	:5 AUG	83 -MODEL 2		
TIME(MIN)	TC=	41	TC=	42	TC-	43
05150505050505050555555555555555555555	37.08555 44.08451 51.08421 51.64421 51.64421 51.62454 51.79875 49.62454 51.82511 55.4976 51.82511 55.4976 51.82511 55.4976 51.82511 52.03628 53.4785 53.4785 53.4785 53.4785 53.4785 53.4785 53.6245 53.6251 5	343; 19957; 199573; 192763 191	44.3999.291.999.3999.3999.3994.44.49999.2097.44.4999.2097.44.4999.2097.44.4999.2097.44.4999.2097.44.4999.2097.4999.2099.2099.2099.2099.2099.2099.2099	6497504 86501965 3107428 3107428 317837492 137837492 137970849 213770849 213770845 213770845 213770845 213770845 21377084 21377084 21377084 21377084 21377084 21377084 21377084 21377084 21377084 213774	37.090638 39.36247 43.0202045 44.075638 44.075638 45.0202045 45.0202045 45.0202045 46.0202045 46.0202045 46.0202045 46.0202045 46.0202045 46.0202045 46.0202045 46.0202045 46.0202045 46.0202045 46.0202045 47.02	759802483 8 3 28 67 88 1 632007 18 32 15 903 8 632007 18

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TIME(HIN)	7C=	44	IC-	45	TC=	46
TIME (MIN) 05.05.05.05.05.05.05.05.05.05.05.05.05.0	27.:3654 39.7177 41.51777 42.848181 43.82183 45.24397 46.14563 46.17563 47.:2897 47.:2897 47.:4132 47.	40714 57143 57	35.77 36.3257 37.737 38.6037 39.6037 40.520340 41.520340 42.60858 43.47542 43.47547 44.5247 44.5247 44.5247 44.87618 45.0138 45.11209 45.0938 45.0938	915374 915374 915374 915327	70 = 39.78194 39.78194 39.78193 41.03493 45.693710 48.974374 49.974374 49.974374 49.974374 49.97449 51.12684 49.974374 49.9844 49.9844 49.9844 49.9843	4 57 4 95 0 5 0 5 0 5 0 5 0 5 0 5 0 5 0 5 0 5
705 735 765	48.0337 48.0455 43.3637	622565	45.2145 45.2405 42.5555	991473	49.5289) 49.50309 38.3131	946298

TIME (MIN)	TC*	47	TC=	48	TC=	49
05150505050505555555555555555555555555	37.26977 40.36674 40.36674 42.8234 43.826999 45.60957 47.6559624 47.6559624 47.6559624 47.6559624 48.60397 49.6039 49	516956 17576 1	36.90277333340.52773639340.527736311446077912.6669770446077912.6669770444444444444444444444444444444444	7287878787887887887887887887887887887887	TC= 34600 42.24600 42.28576 46.7576 46.7576 46.7576 46.7576 47.2676 47.2676 47.2676 47.48.0326 47.49.0326 48.49.0326 48.666778 48.656678 48.656678 48.656678 48.656678 48.656678 48.656678 48.656678 48.656678 48.656678 48.656678 48.656678 48.656678 48.656678 48.656678 48.656678 48.656678 48.656678	0.000
495 525 555	49.1296 49.1323 49.1182 49.0924	629304 795361	46.0178 46.0391 45.3611 45.9493	578847 949527	49.0469 48.9858 48.3683 48.8448	50793 224895 -
585 615 645 675 705 735 765	49.1112 49.1276 49.1863 49.2074 49.2332 43.6670	377957 685051 459853 683691 805313	46.0462 46.07462 46.1360 46.1454 46.1454 46.18406	448718 919016 054258 530482 419064	48.9317 48.9999 49.2537 49.1245 49.1245 43.7004	908721 52499 219147 020393 020393

TIME(MIN)	TC*	50	TC=	51		TC=	52
05 105 0 5 105	TC = 20018	229525:159438351952 988438151952 9884381212843512952 9884381212843512952 9884381312851952 98843812851952 98843812851952 98843812851952 988438132952 988438132952 988438132952 9884381381 9884381381 9884381381 98838	TC = 03285 77.03285 033885 033885 033885 033885 033885 0340.12885	249 249 2217897 2217897 2217897 2217897 2217897 2217897 2217897 2217897 2217897 2217897 2217897 22188463 2218846	08245566777778887888888899999888888888888888	.5672 .5572 .5572 .5538 .508 .619 .619 .619 .619 .619 .619 .619 .619	0.6777845::04 :::33373835:55 5 :957:77:8:8 6704831255406368:3455459:55:56550767 6704831255406368:3425344:0635:73567 6704831255406368:3425344:0635:7367 6704831255406368:342554 6705831783178387 6705831783178318 6705831783178318 6705831783178318
735 765	45.8782 43.2610		50.2478 44.2317	622515		.04749 .99562	

TIME (MIN)	TC=	5 3	TC=	77
0 5 10 5 10 5 10 5 10 5 10 5 10 5 10 5	37.8480 37.7735 37.7663 37.7663 37.7711 37.5838 36.8938 36.8938 37.0553 37.1944 37.224 37.224 37.224 37.324	1201914 187373 1803616 1804473 192567 19379547 180007 1899464 1894473 18544445	37.402167886838.55168585838.55168585838.551685858388.39.66029.56029.56029.60029.66029.66029.60029.60029.60029.60029.60029.60029.60029.6002	996 1997 1

TIMECHIND	TC=	51	TC=	62	TC=	63
051595050505050555555555555555555555555	66,3815	3641 3678 3678 3678 3678 3678 3678 3678 3678 3678 3678 3678 3678 3678 3688	51.25.36.22.36.36.36.36.36.36.36.36.36.36.36.36.36.	4141247 099123 8042136 8042136 8042136 8042136 80426127 66627 66	48.029444 57.3431966 48.5943196 48.5943196 48.	71748757840707171877850317408757840707071877487578407070718774388087584070707187485748574857840707071877488657385748578850977468657385748578857746865774686577468657746865774686577468657746866777468667770070868677746866777007086867774686677700708686777468667770070868677746866777007086867770070868677700708686777007086867770070868677700708686777007086867770070868677700708686777007086867770070868677700708686777007086867770070868677700708686770070868677700708686777007086867770070868677700708686777007086867770070868677700708686777007086867770070868677700708686777007086867700708686777007086867770070868677700708686777007086867770070868677086867770070868677086867770070868677700708686777007086867770070868677700708686770868677700708686770868677700708686770868677086868677007086868677086868686

TIME (MIN)	TC=	54	TC -	65	TC	* 56
0511223344555667711112223334445555666777705555555555555555555555555	41.009.769.895999.50.009.769.769.769.769.769.769.769.769.769.76	48852500	53.444.533.7344.535.535.535.535.535.535.535.535.535.	99.69.59.4479 154.69.69.69.69.69.69.69.69.69.69.69.69.69.		5.5 7. 0.4 4. 5. 0.4 . 5. 5. 5. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6.

0 45.395808997 44.4571194196 37.5832756 5 38.5487756192 55.1603900256 42.4533057 10 42.6176859684 58.3972974901 45.3295164 15 44.4883932526 60.9578703934 47.9281623 20 41.6768240704 53.8815371362 49.1547803 25 46.5143351390 58.2273570767 49.3976463 30 49.4279425344 58.1625706069 50.2410143 35 42.3977400955 58.14405893293 50.689658	53645 57157 54015 23404 01163
20 41.8768290704 59.881537:062 49.16476025 25 46.514395:290 58.2272570767 49.1976463 30 49.4279426784 58.1625706069 50.6296561 40 43.1176862552 58.1440589299 51.496361661 40 43.1176862552 58.1440589299 51.496361661 50 51.255766:17 58.3869779045 51.4943157 50 51.255766:17 58.3860779779 51.49622 51.49636561 60 42.6368942546 59.1083856299 52.277778 61 41.0574520393 59.4799854353 52.277778 65 43.44061815772 59.304506299 51.29627 52.27778 65 43.44061815772 59.304506299 52.27778 66 41.0574520393 59.4799854353 52.533095 67 41.0574520393 59.4799854353 52.533095 68 43.44061815772 59.306562399 52.27778 69 41.0574520393 59.4799854353 52.533095 60 42.636892544 59.505079237 52.7254494 61 1813847906 59.505079237 52.7254494 61 1813847906 59.505079237 52.7254494 62 41.1813847906 59.505079237 52.7254494 63 41.1813847906 59.505079237 52.7254494 64 1.89864267759 59.3876356011 53.273024 64 1.898642677769 59.3876356011 53.273024 65 41.1813847906 59.3876356011 53.273024 65 41.18186557769 59.3876356011 53.273024 65 41.0836709779 59.3876356011 53.282664 67 41.0836709779 59.387676564 53.382666 67 42.530114887 59.38307718096 59.382666 67 44.6657715933 59.3836776379 59.383666 67 44.945657715933 59.3836776379 59.383666 67 44.95657715933 59.3836776379 59.383666 67 44.96567715933 59.3836776379 59.383666 67 44.6657715933 59.3836776379 59.383666 67 44.6657715933 59.383677639 59.326666 67 44.6657715933 59.3836776379 59.383666 67 44.6657715933 59.3836776379 59.385666 67 44.6657715933 59.38518459179 59.326666 67 5 44.045657715933 59.385184591793 53.366666 67 5 44.6656715933 59.385184591793 53.366666 67 5 44.6657715933 59.385184591793 53.366666 67 5 44.6656715933 59.385184591793 53.366666 67 5 44.6656715933 59.385184591793 53.366666 67 5 44.665671156672 59.3853407203 53.1851567 68 59.38541156672 59.3853407203 53.1851567 69 59.38541156672 59.3853407203 53.1851567 69 59.38541156672 59.3853407203 53.1851567 69 59.38541156672 59.3853407203 53.1851567 69 59.38541156672 59.3853407203 53.1851567 69 59.38541156672 59.3853407203 53.1851567 69 59.385411566	

TIME (MIN)	īC=	70	TC -	71	ĩC•	72
05112233344505050505055555555555555555555555	38.12077 50.775 13077 50.10133 47.9017 50.10133 51.12134 51.12134 51.12134 51.12134 51.12134 51.1213 5	62024478+532+73856 62024478+532+7966647646 62024478+532+7966647646 62024478+532+7966647646 6202442478+532466647646 6202424878+532466647646 6202424866477696486647646 620244866476486 620244866486486 62024486 62024486 62024486 62024486 62024486 62024486 62024486 62024486 6202486486 620248	4.3356544;0044670970978445658448847508475355549490846709765799784456571298847509445657129844750847508	18	4.14 4 99 6 70 5 16 7 916 8 5 7 70 6 10 10 10 10 10 16 14 4 97 6 7 10 8 4 16 12 5 7 16 7 7 16 7 16 8 7 16 7 16 7 16 7 16	1

TIME(MIN)	TC=	73	TC+	79	10+	90
05112233344505050505555555555555555555555555	36.757811 75.78151 75.78	25.24000 25.240	37.5685 37.595 37.695 37.973 36.8973 36.8973 37.11344 36.8973 37.11344 37.11344 37.1235 37.1235 37.1235 37.1235 37.337	1727522 2534414 27290023 193548 19354958 1175415 105677415 105677415 105677415 105674415 105674415 105674415 105674415 105674415 105674415 10567445 105674 1056744 105674 105674 105674 105674 105674 105674 105674 105674 10567	41.79792 41.5975 41.6356 41.7665 41.3569 41.3801 42.02110 42.0870 42.1092	144

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